

# High-fidelity aerodynamic shape optimization for wind turbines

Tristan Dhert

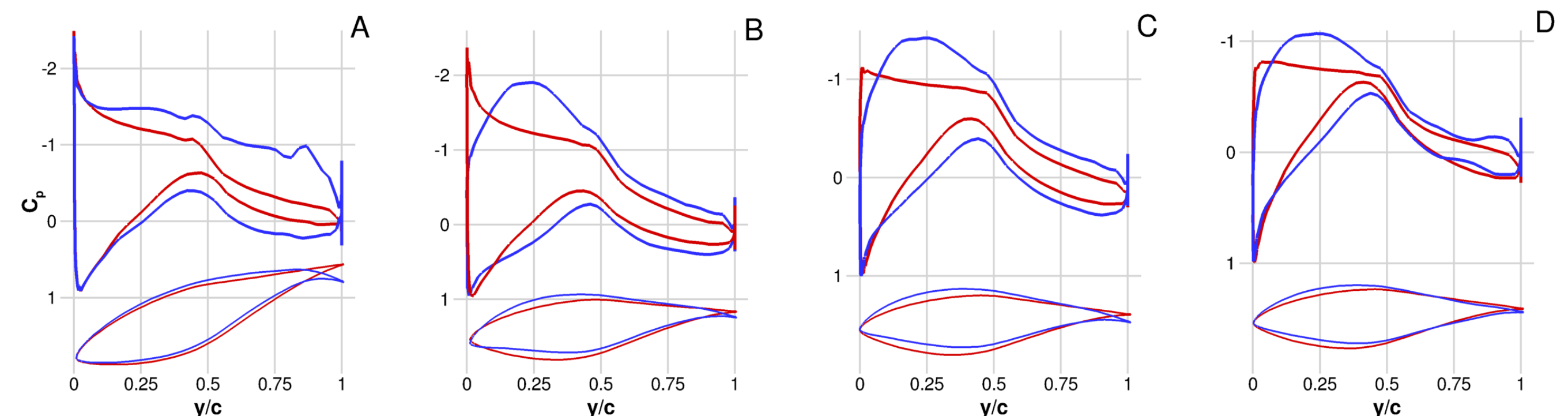
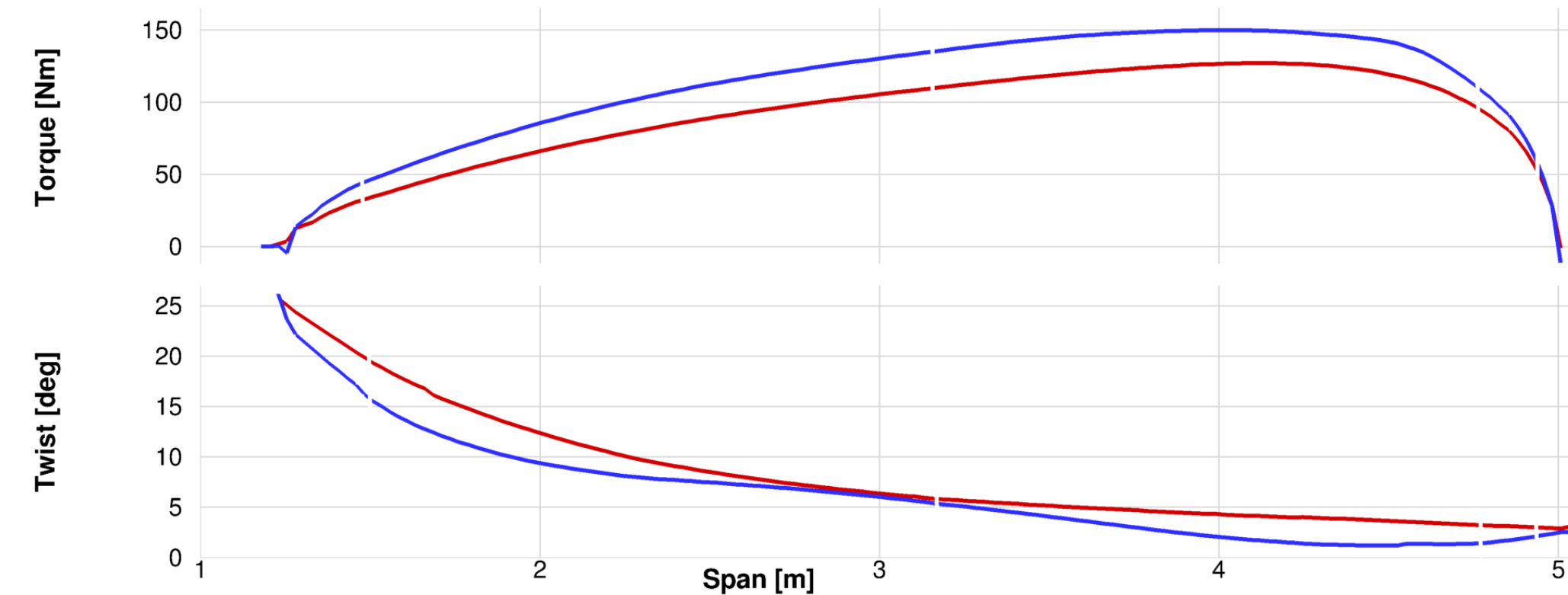
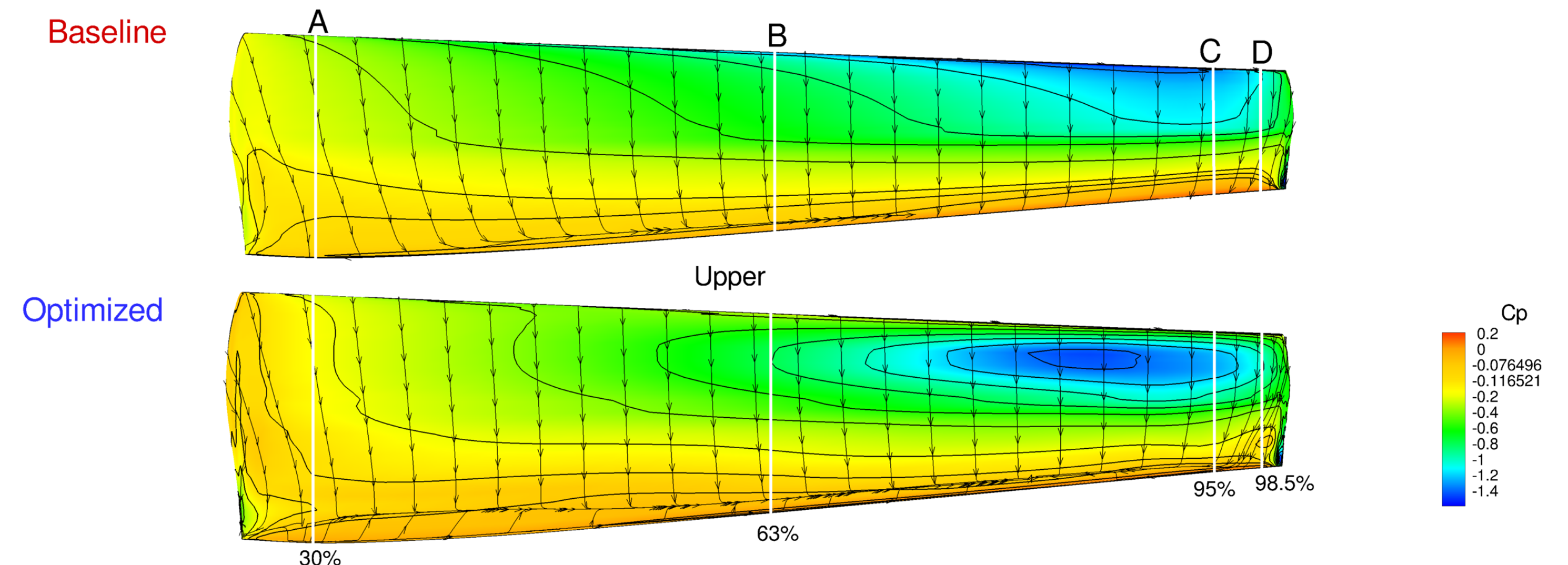
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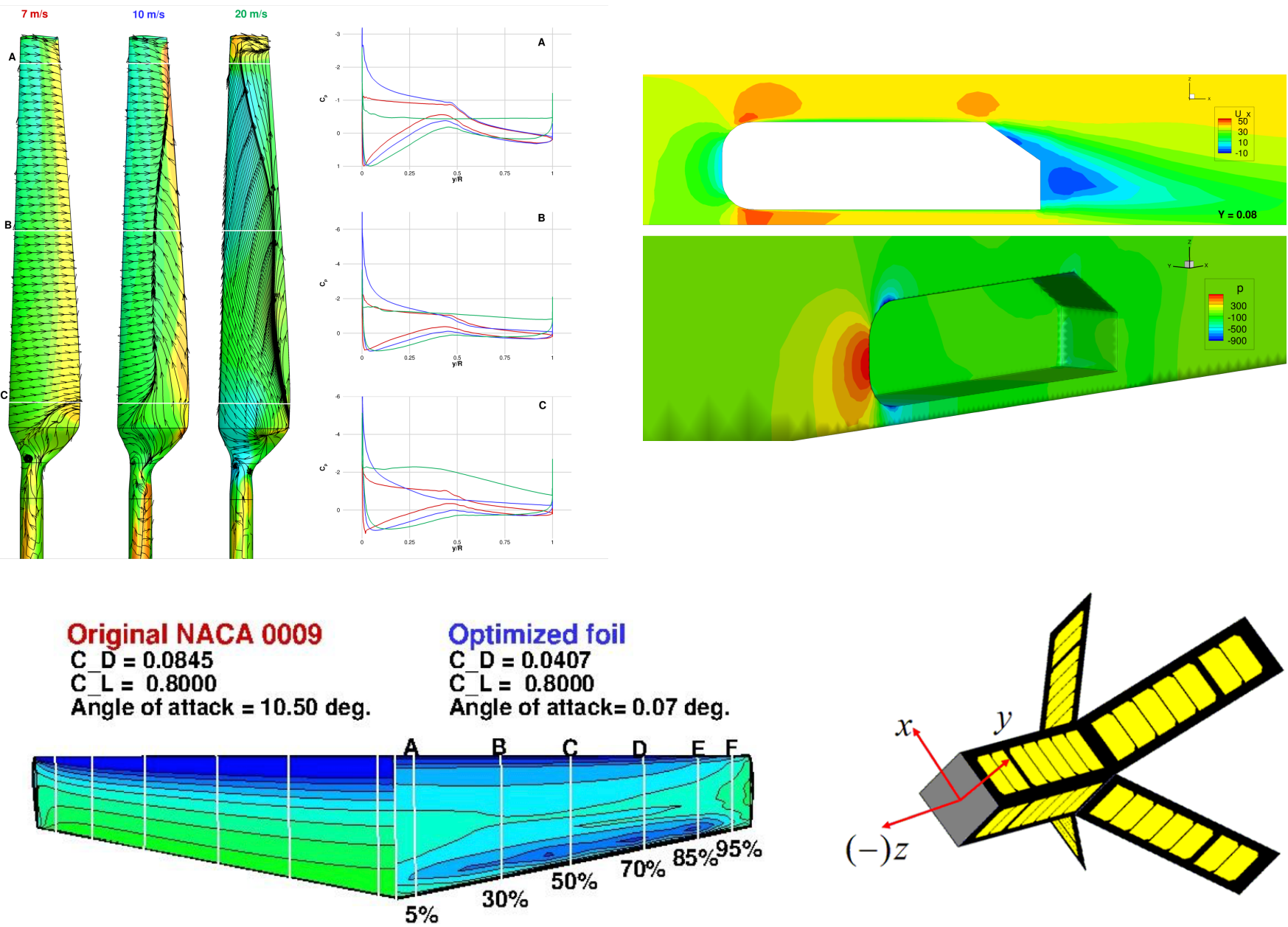
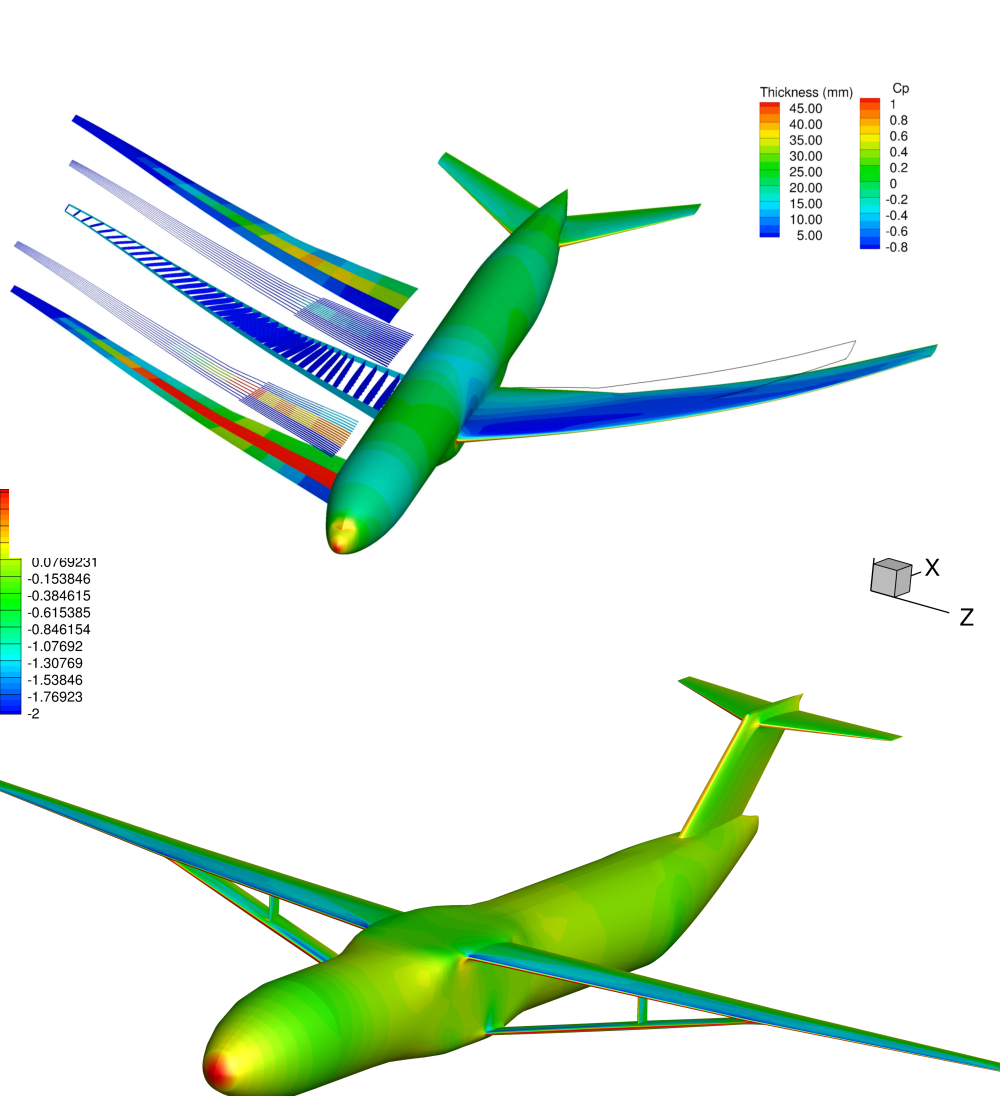
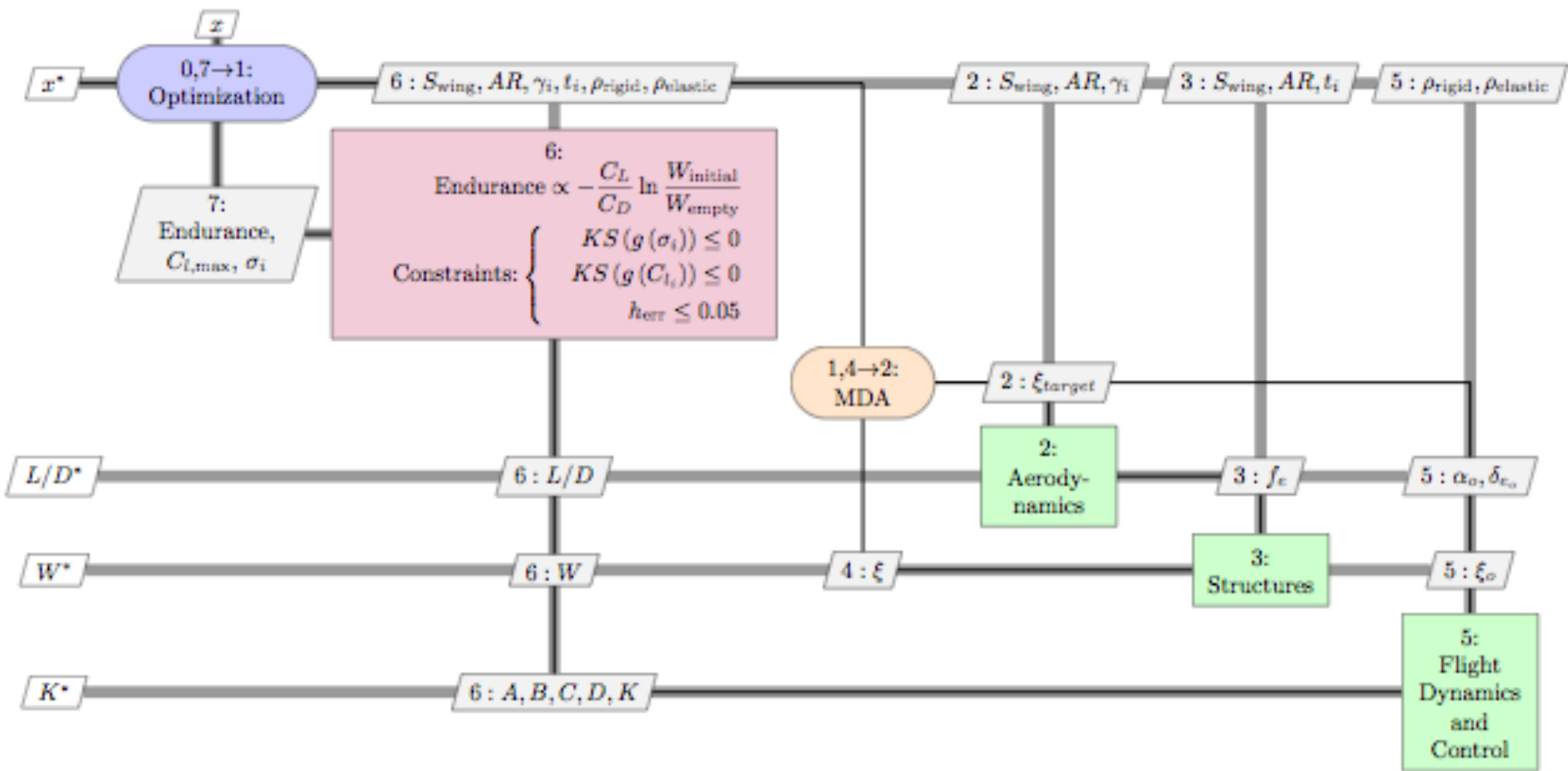
Newsletter: MDOLab



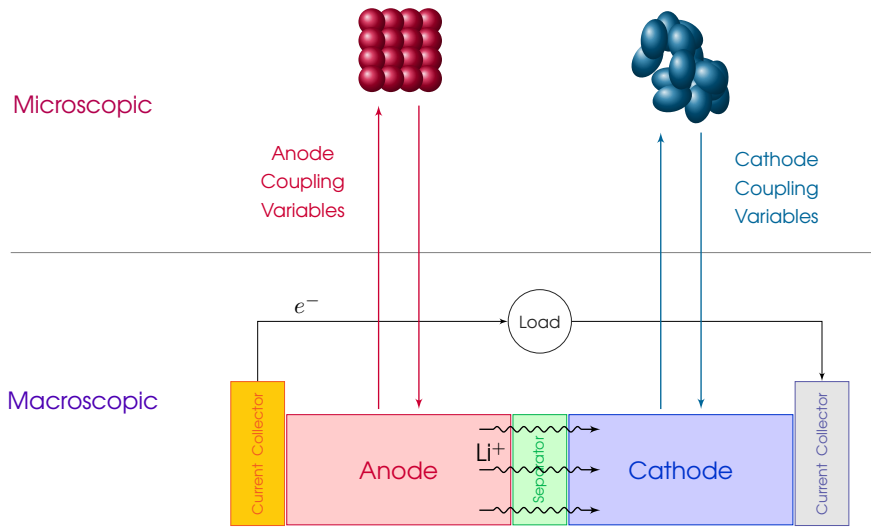
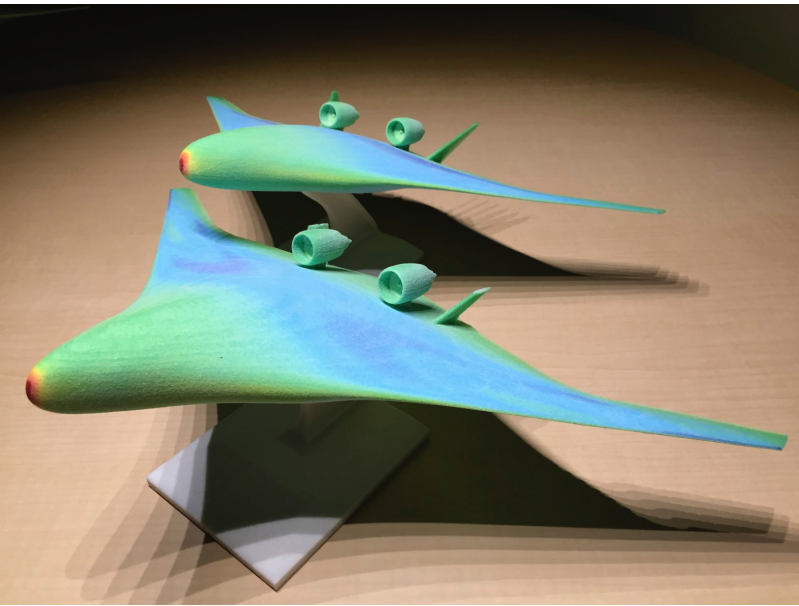
# MDOlab research is divided into two main thrusts

Fundamental MDO algorithms

Applications of MDO

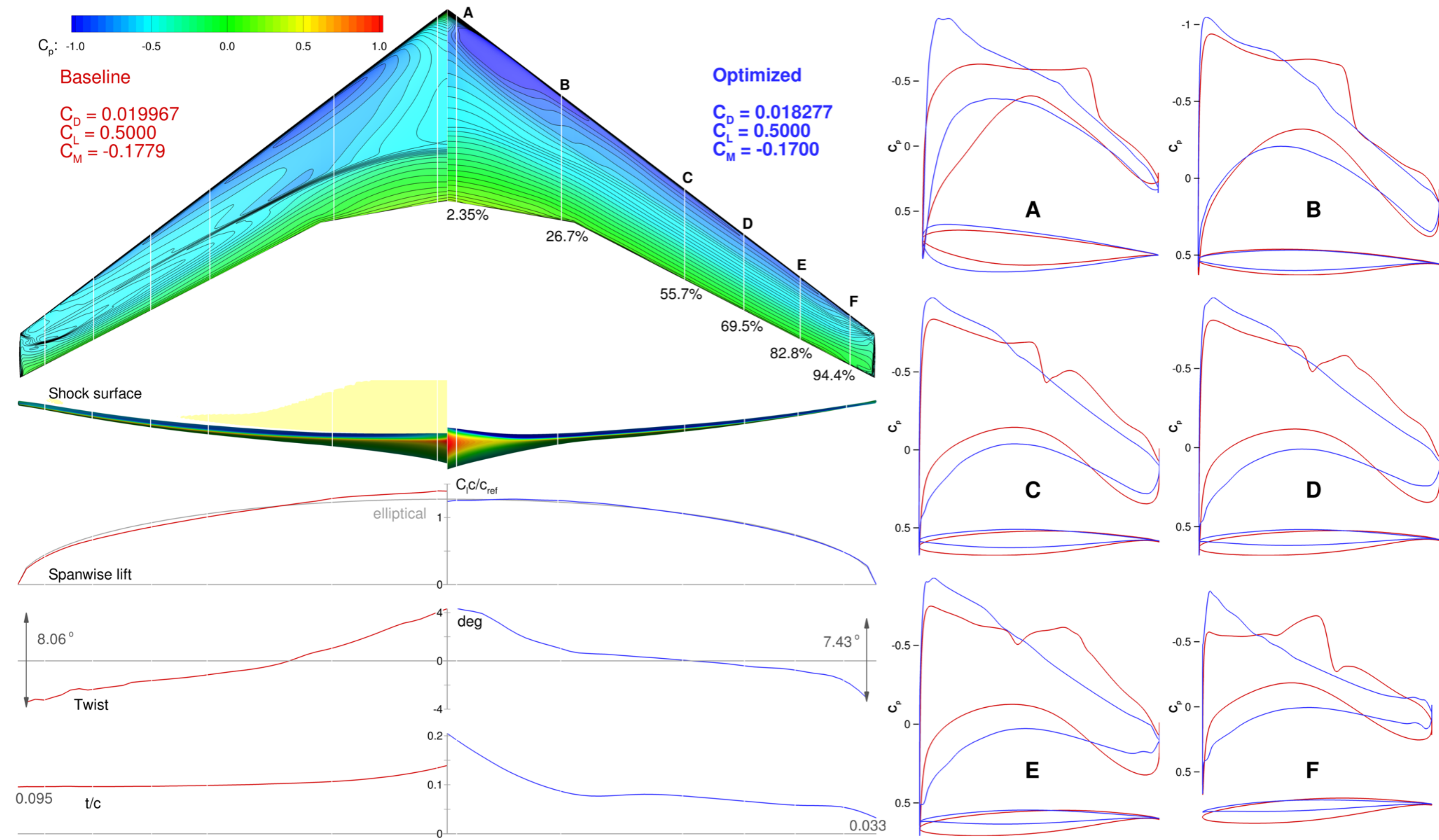


$$\frac{\partial R}{\partial u} \frac{du}{dr} = \mathcal{I} = \left[ \frac{\partial R}{\partial u} \right]^T \left[ \frac{du}{dr} \right]^T$$



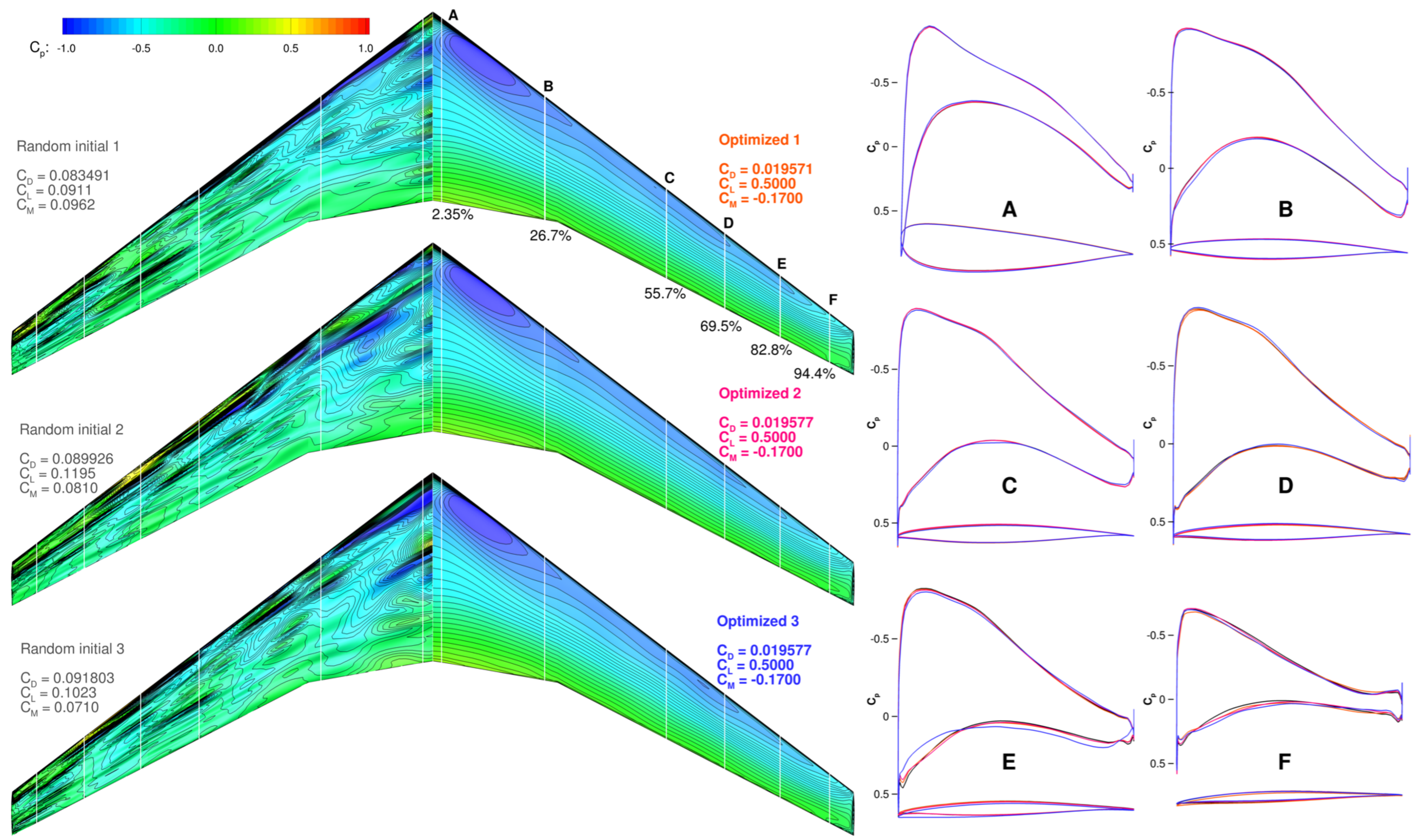


# Optimization can refine good designs...



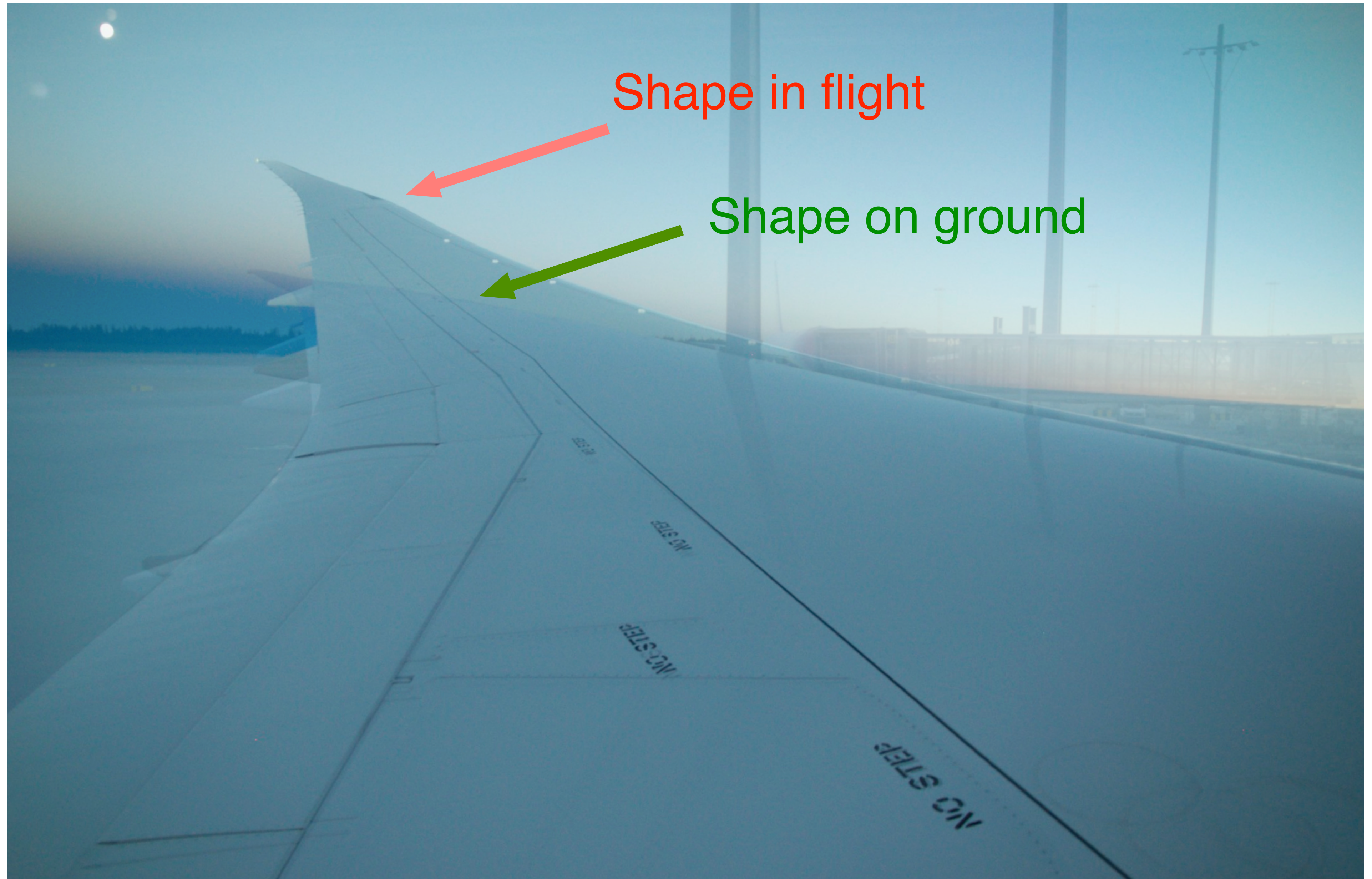


...but can we start from really bad designs?



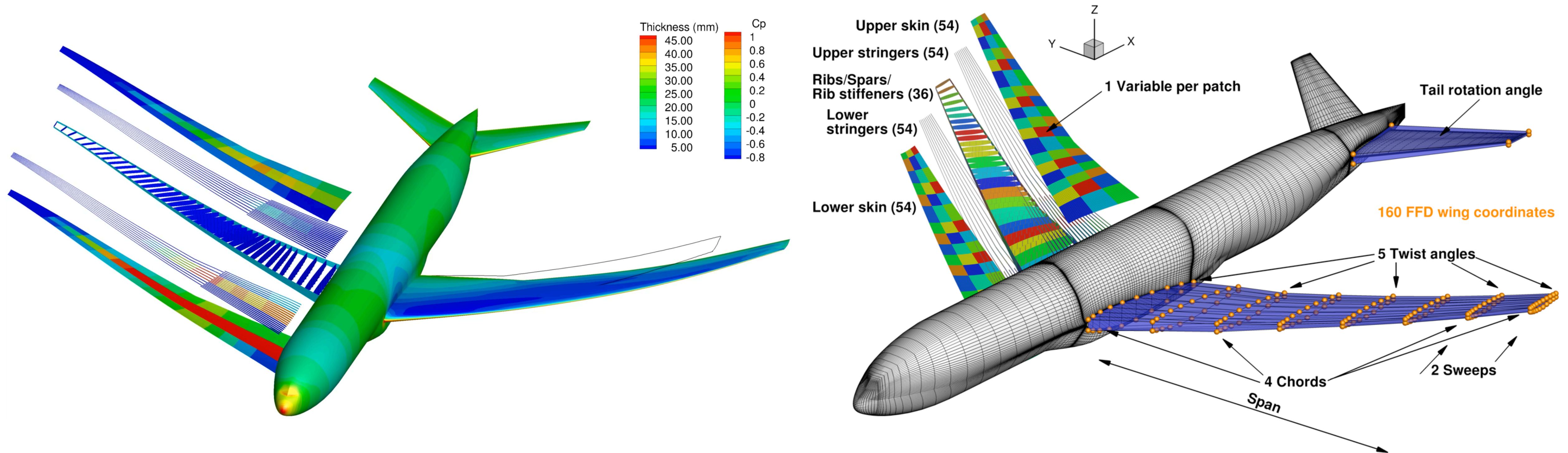


# Wing design demands more than just aerodynamics





# Want to optimize both aerodynamic shape and structural sizing, with high-fidelity

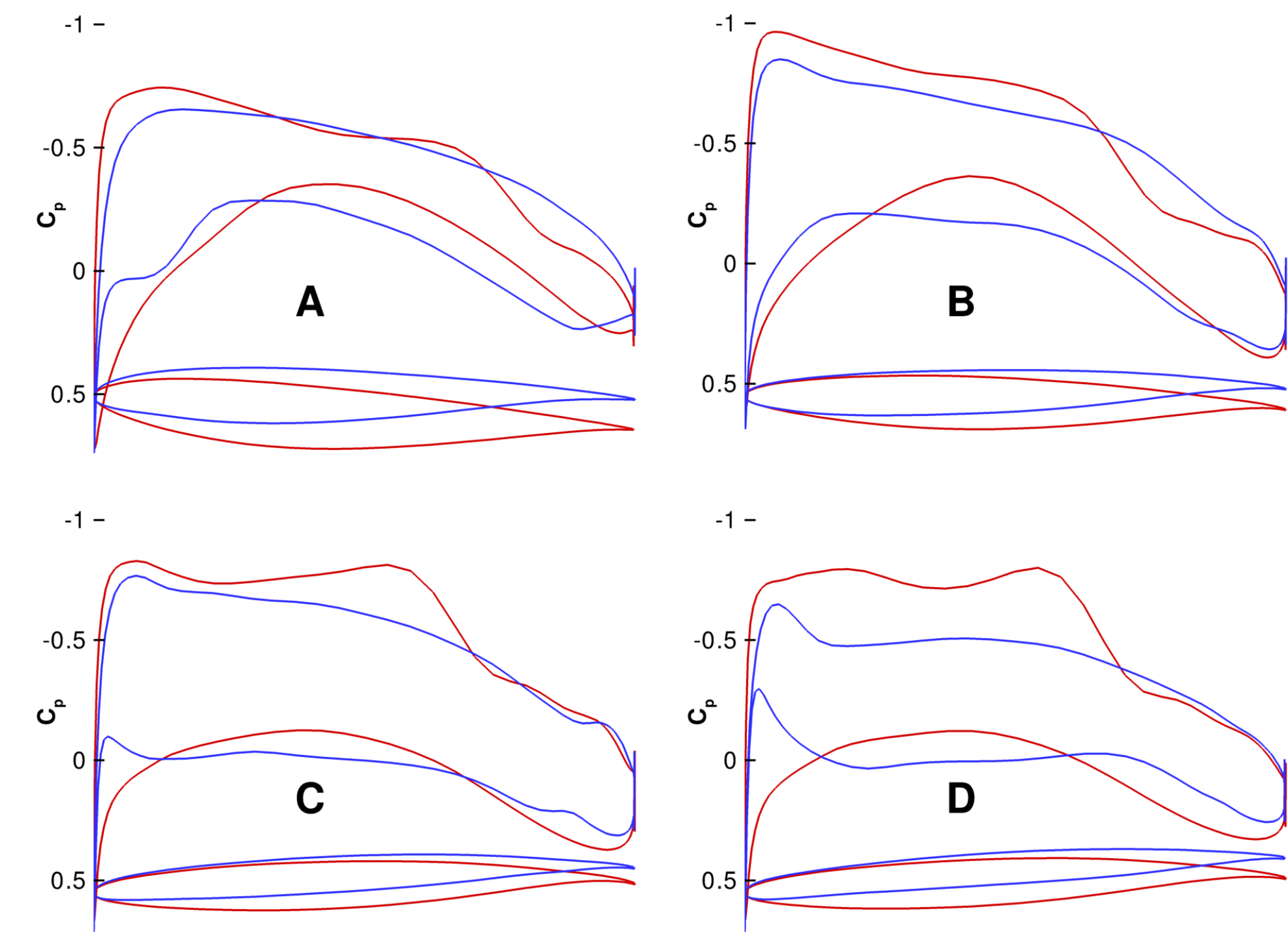
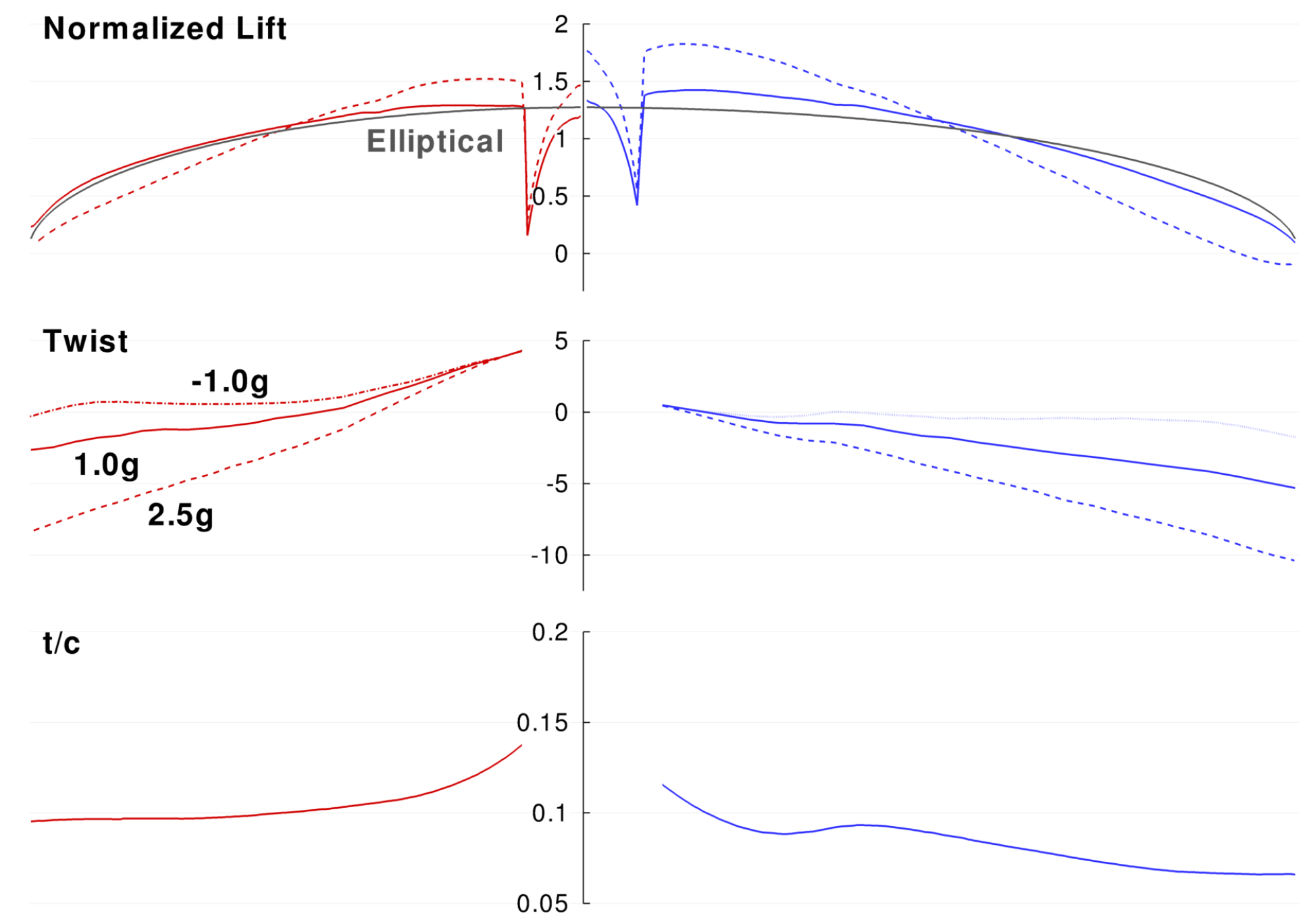
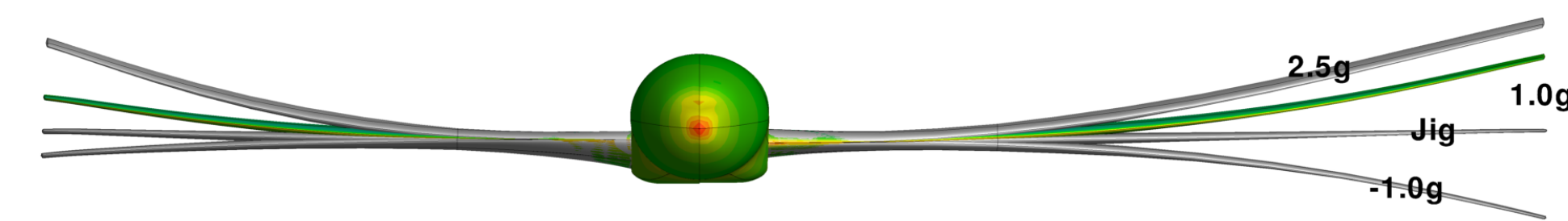
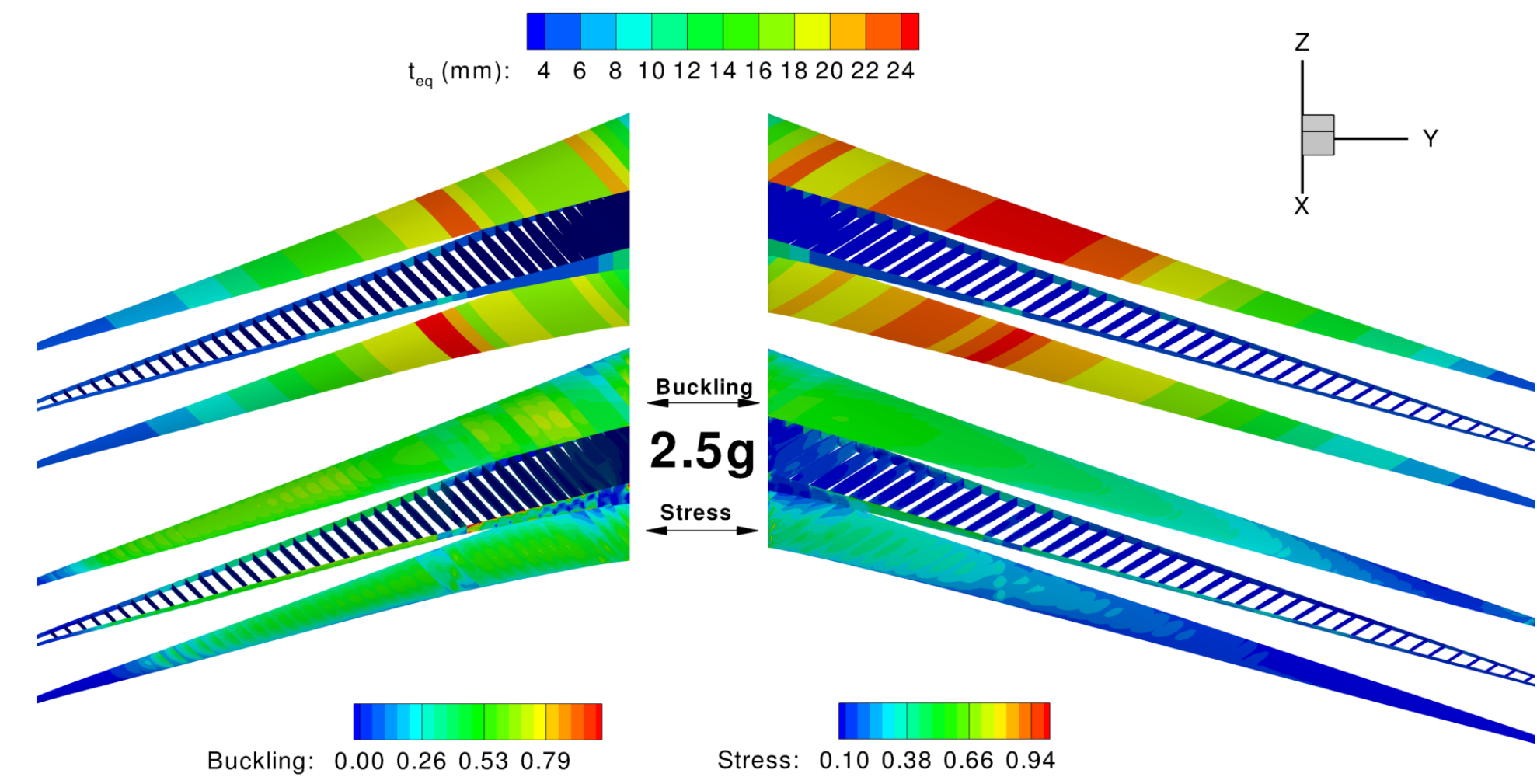
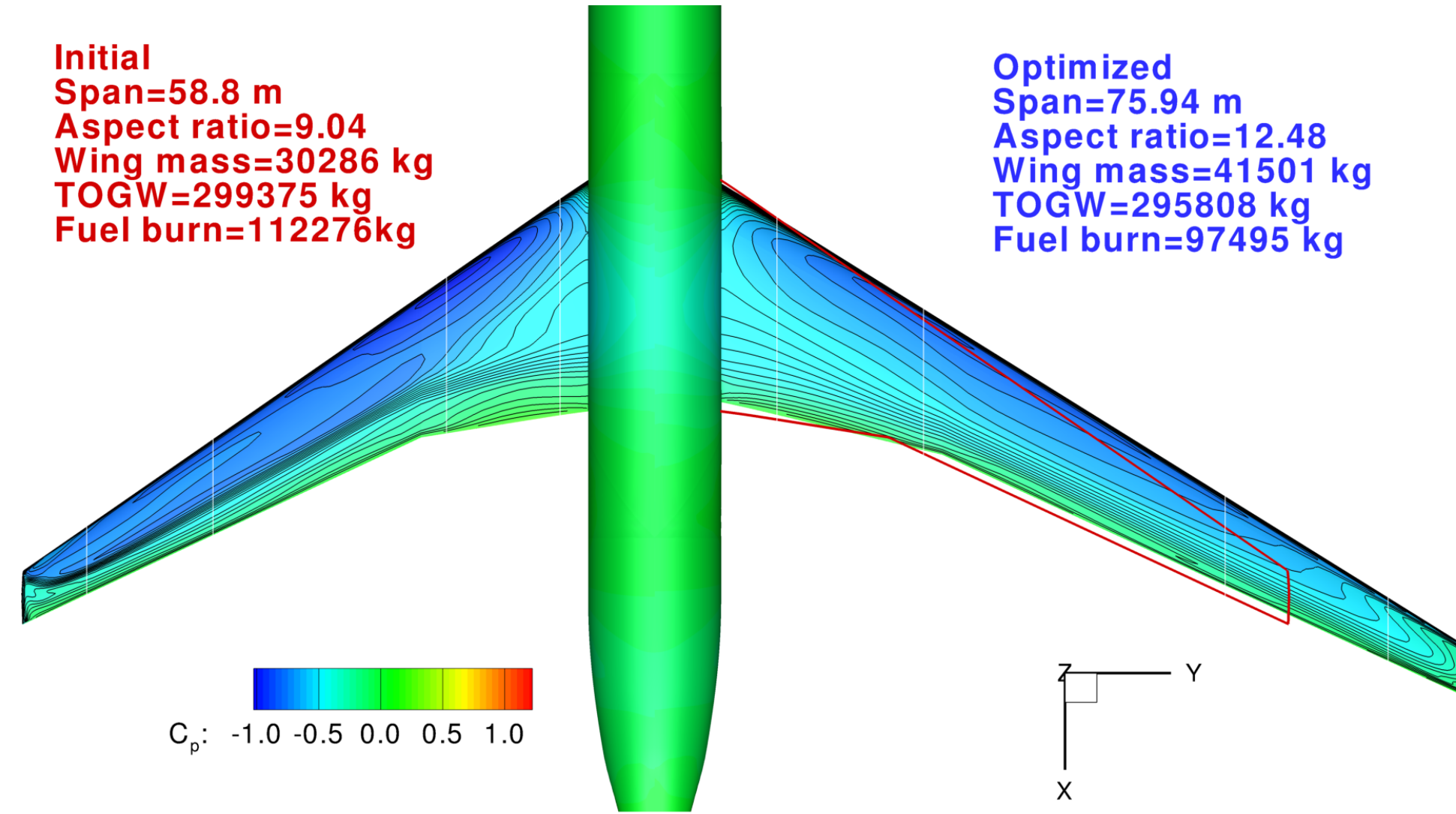


[Kenway and Martins, J. Aircraft, 2014]



Initial  
Span=58.8 m  
Aspect ratio=9.04  
Wing mass=30286 kg  
TOGW=299375 kg  
Fuel burn=112276kg

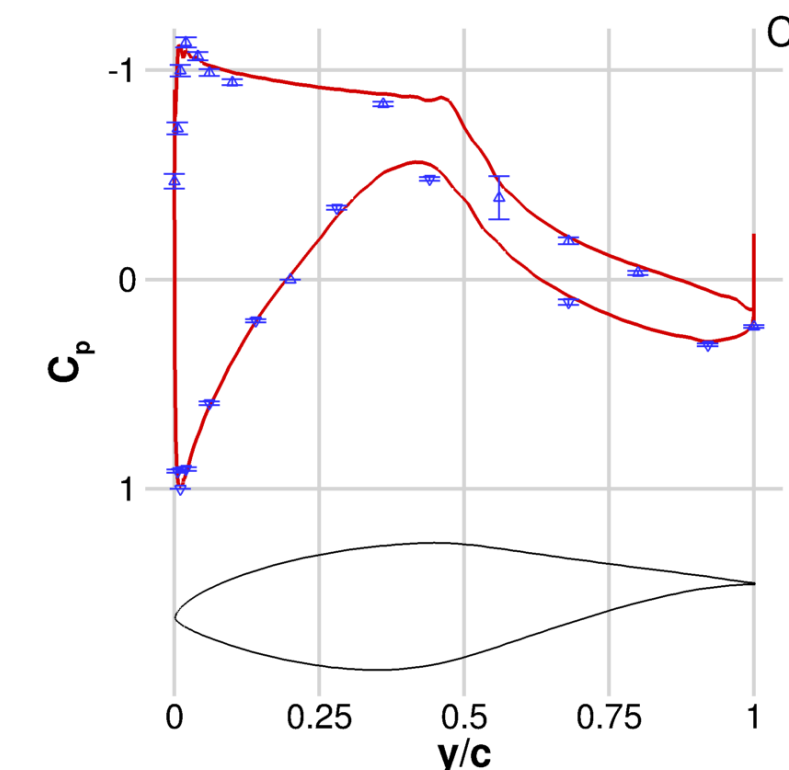
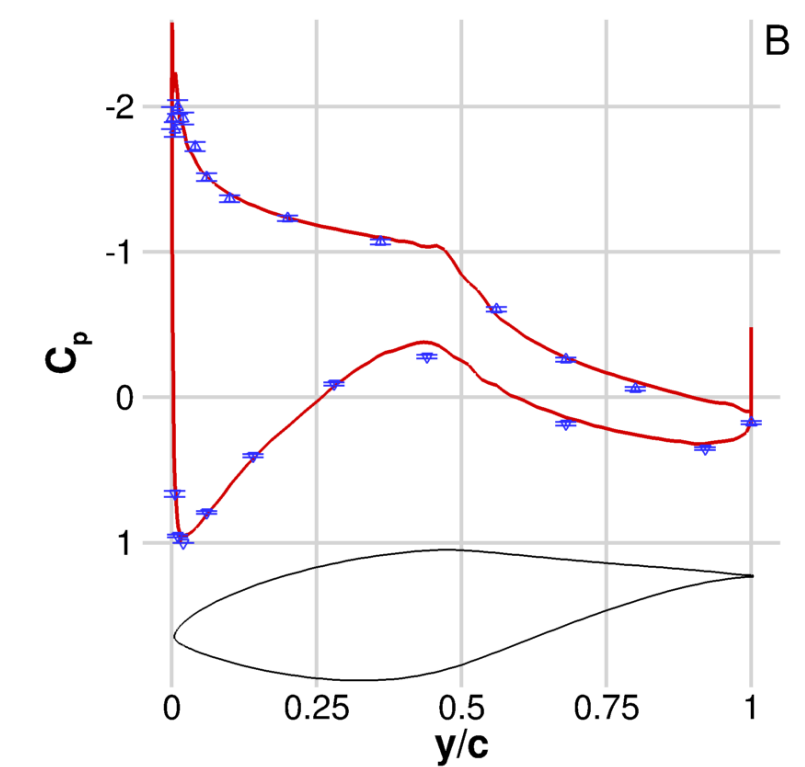
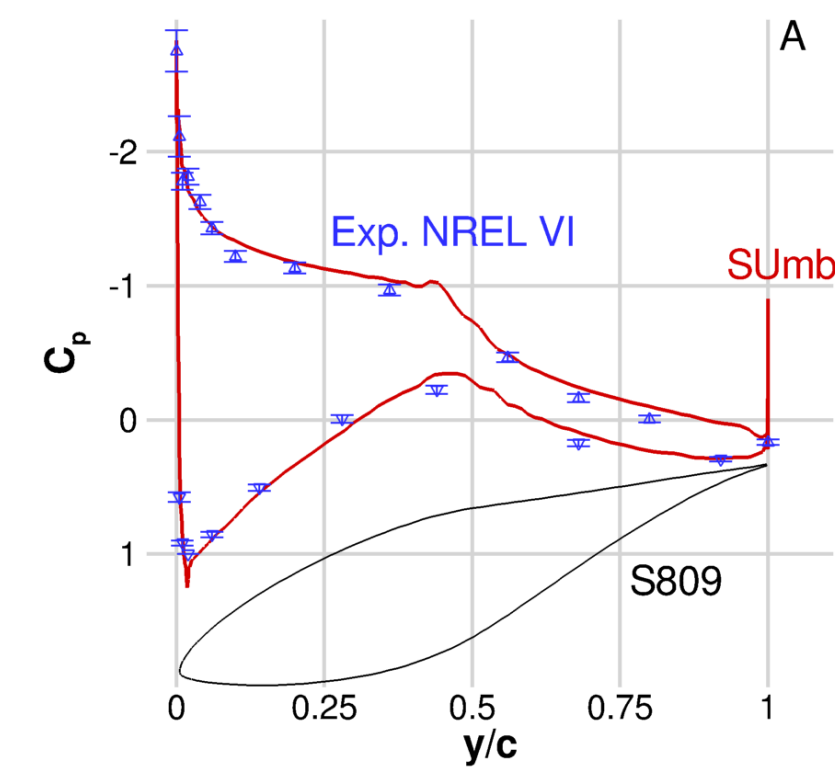
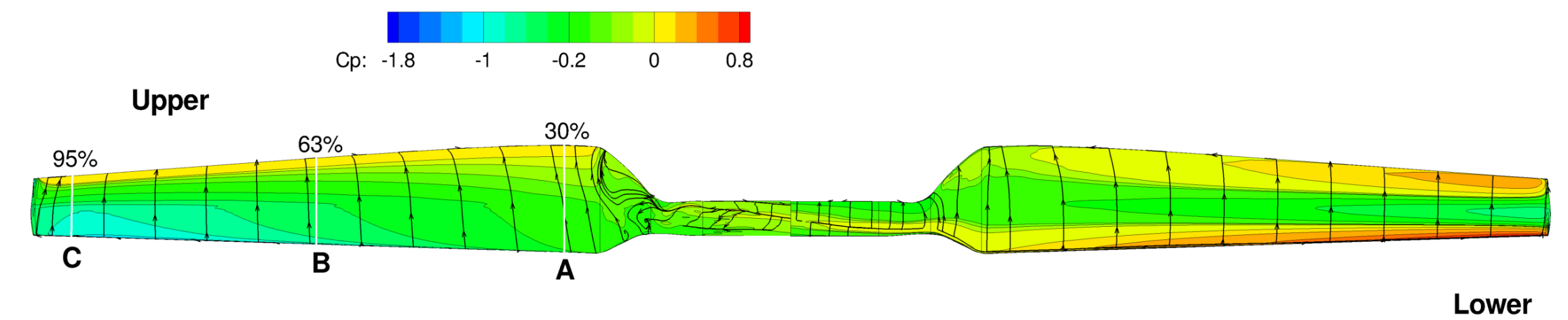
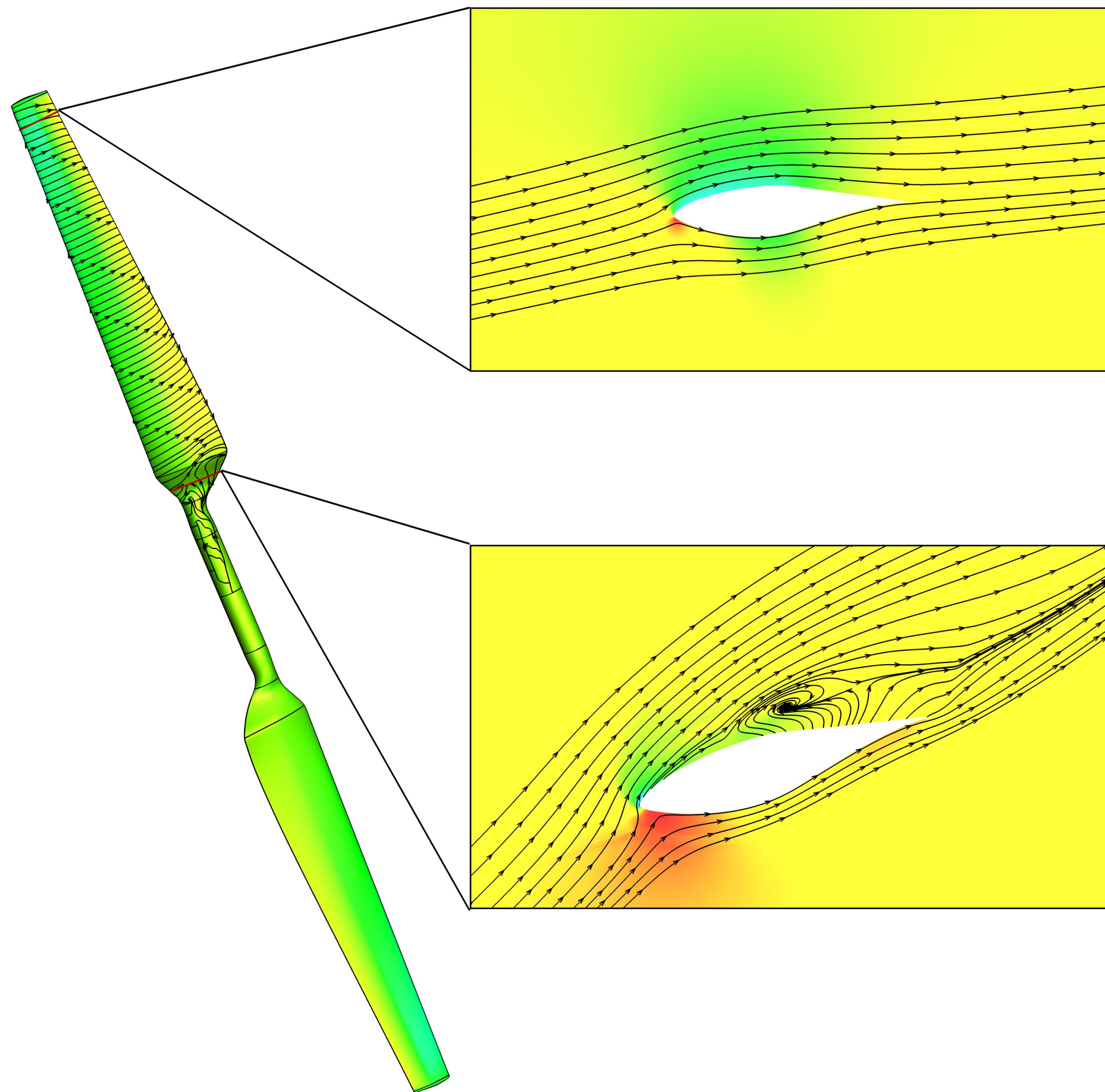
Optimized  
Span=75.94 m  
Aspect ratio=12.48  
Wing mass=41501 kg  
TOGW=295808 kg  
Fuel burn=97495 kg



[Kenway, Kennedy, and Martins, AIAA J., 2014]



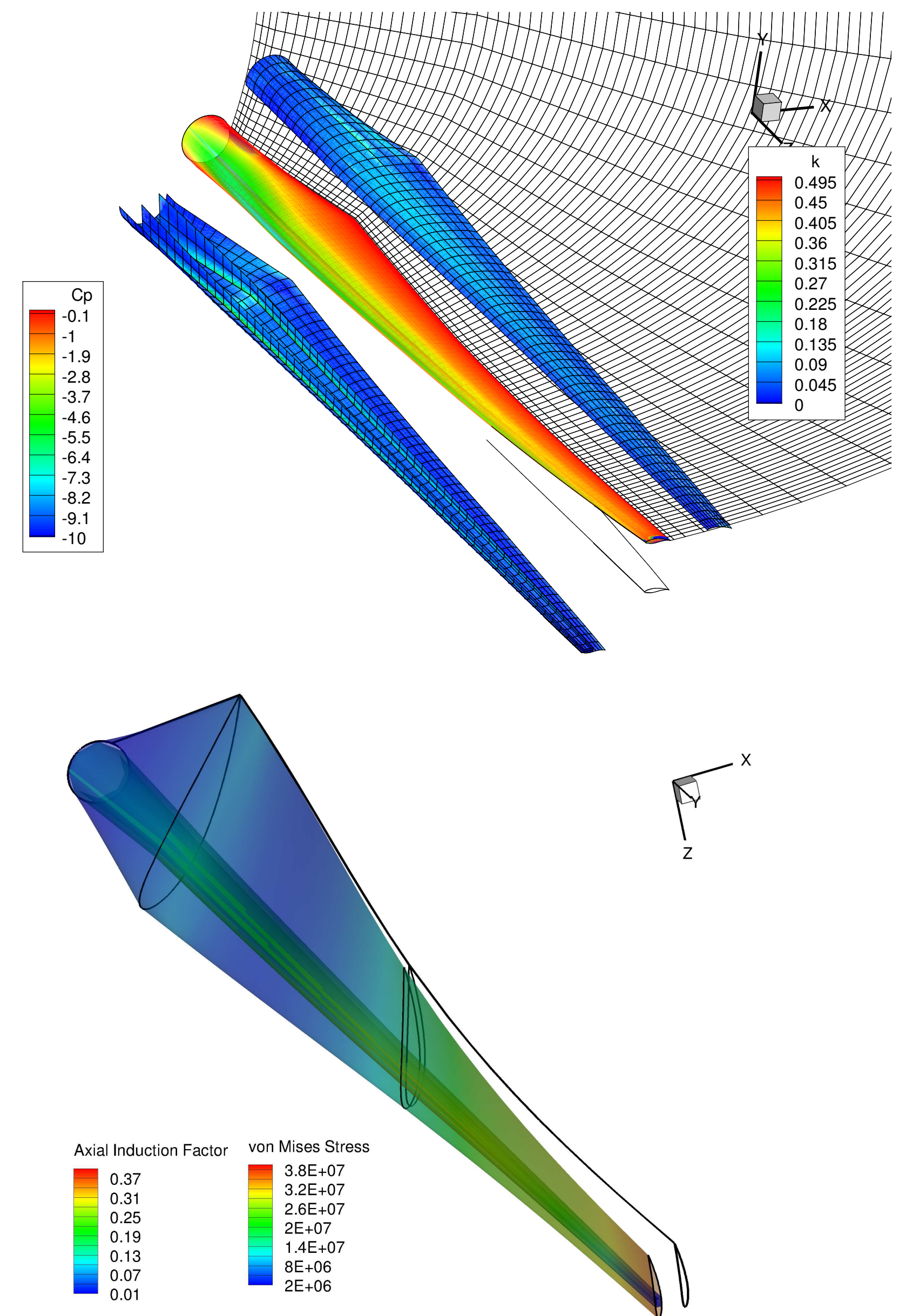
# This aerostructural optimization framework can be adapted for the design of wind turbine blades





# Our previous effort were limited to low-fidelity aerodynamic models

- Aerostructural analysis using 3D panel method and FEM
- Aerostructural optimization with BEM theory and beam finite elements
- Aerodynamic shape optimization by use of BEM theory

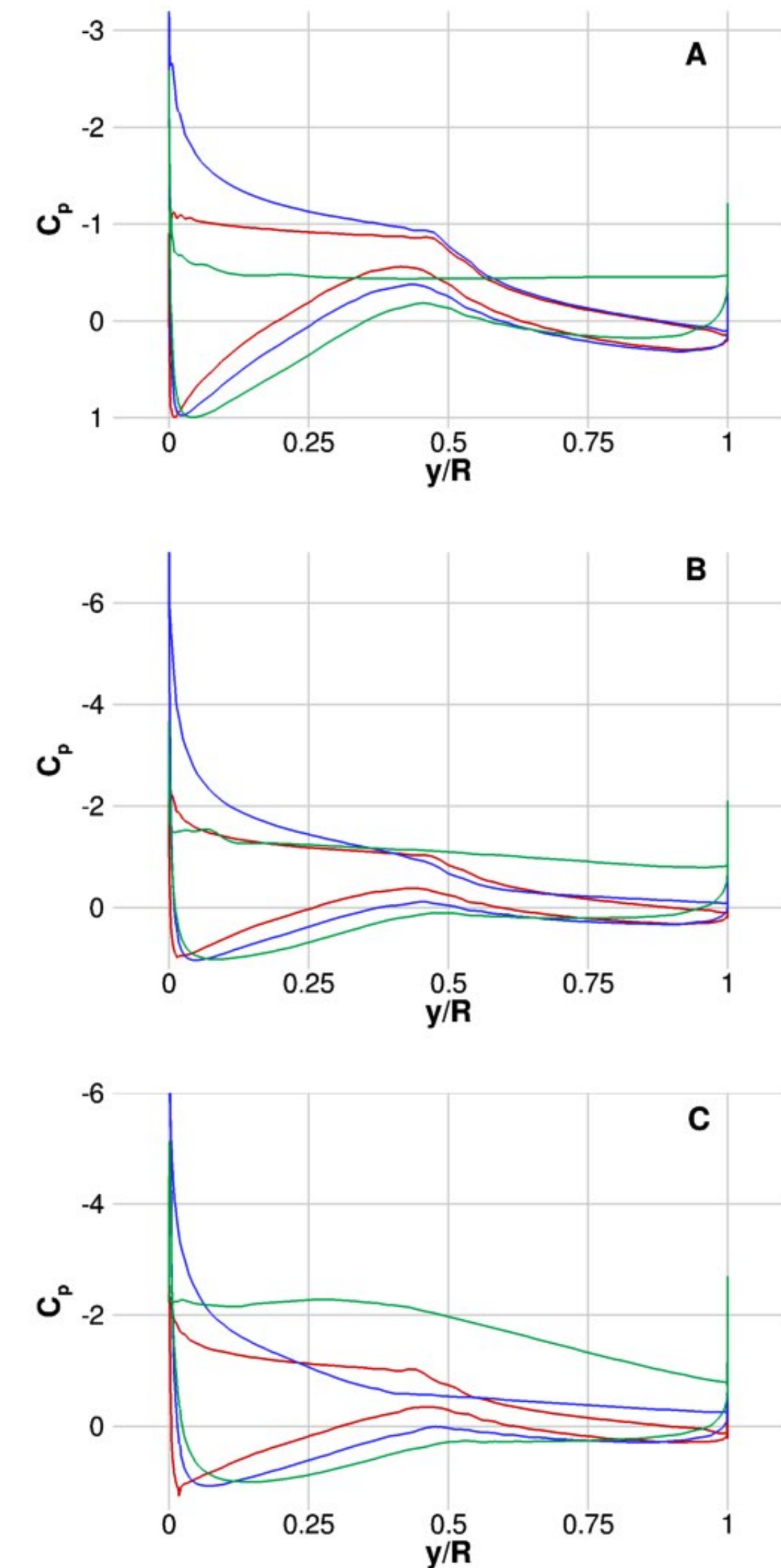
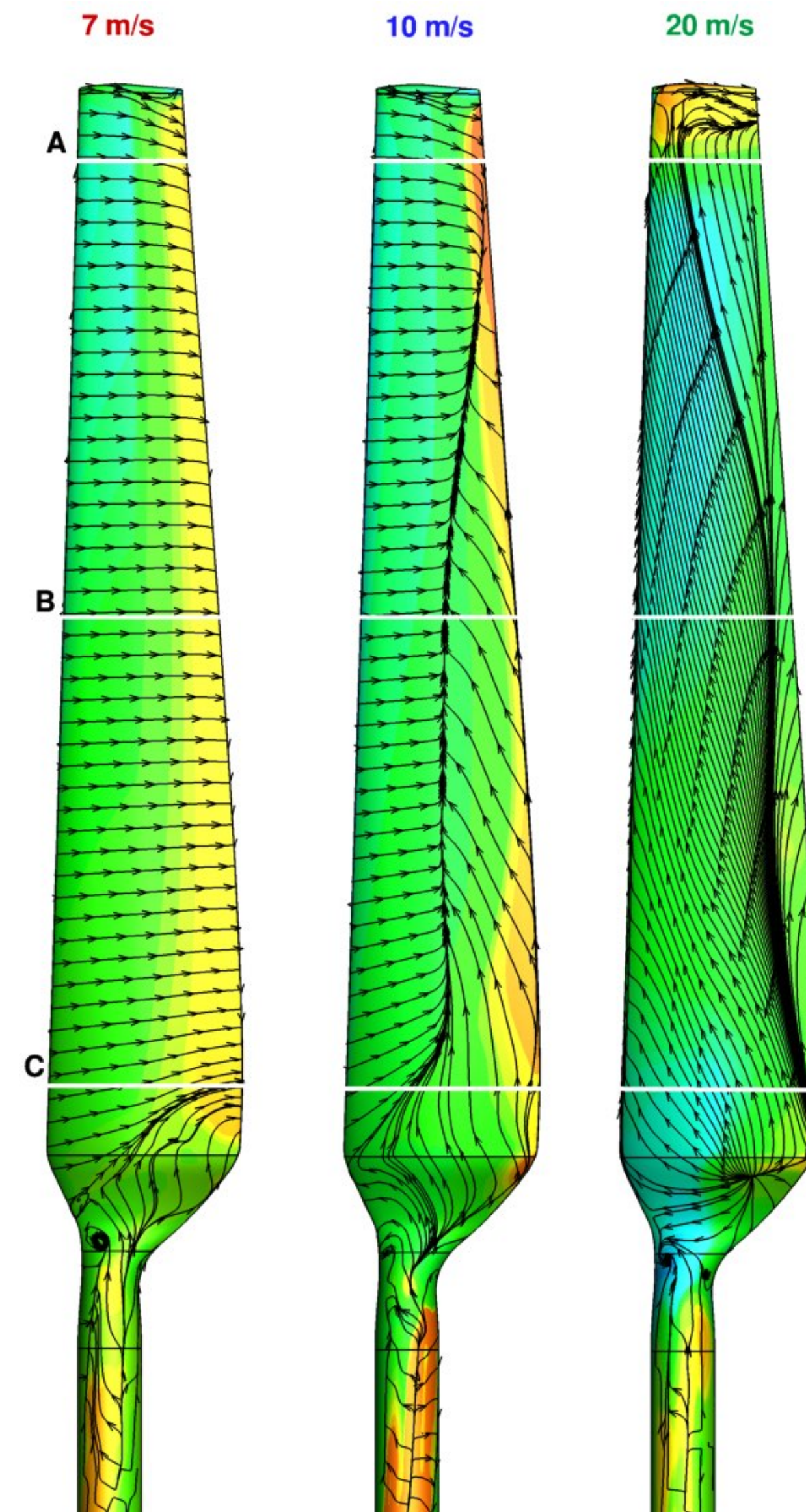


[Kenway and Martins, AIAA J., 2008]



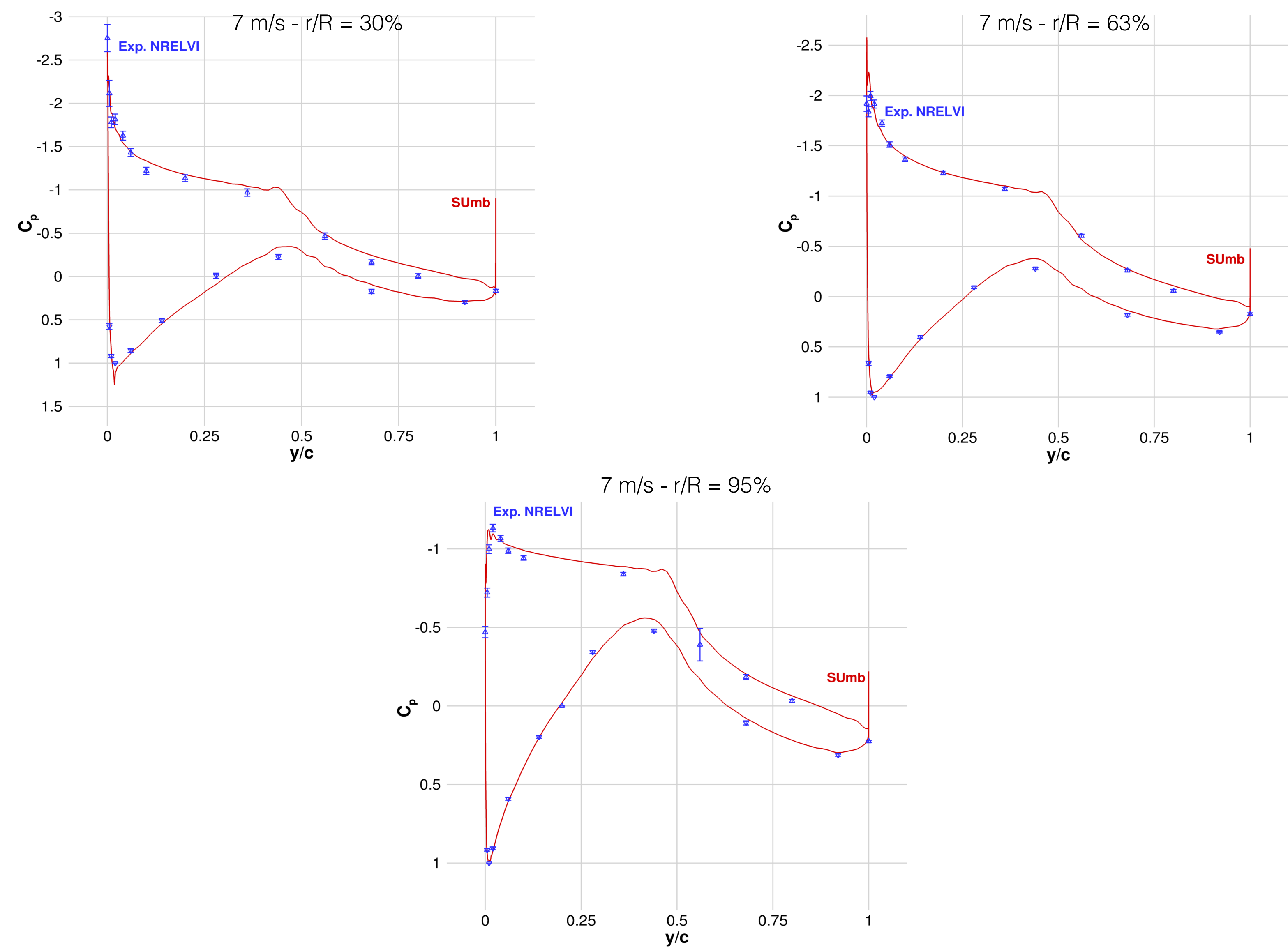
# We can now perform steady-state RANS analysis in the rotating frame

- Structured compressible RANS-based solver 'SUmb'
- Roe scheme without limiter
- Spalart–Allmaras turbulence model
- Wind speeds: 5, 7, 10, 13, 15, 20, and 25 m/s



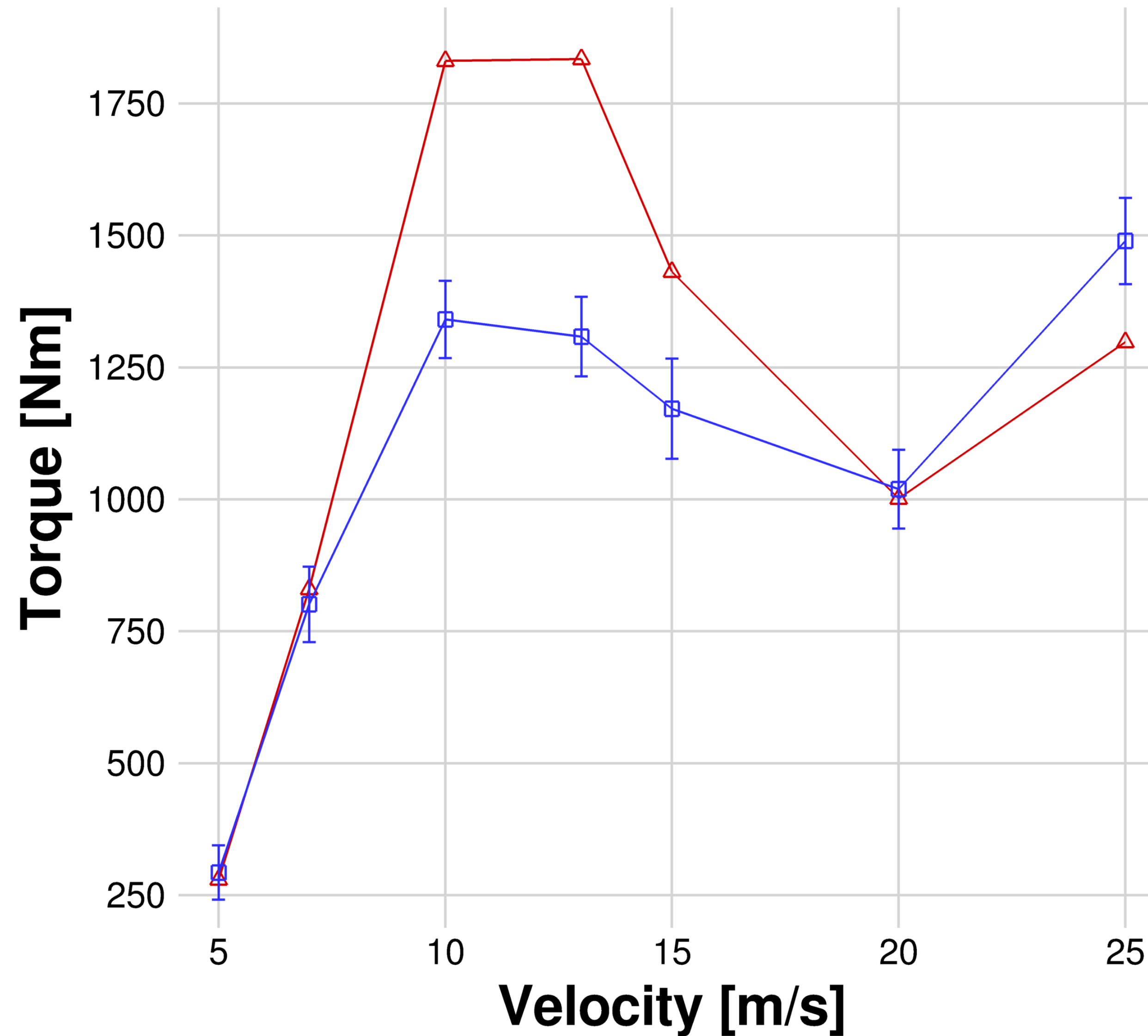


# Attached flows are well predicted for the NREL VI sequence S experiment



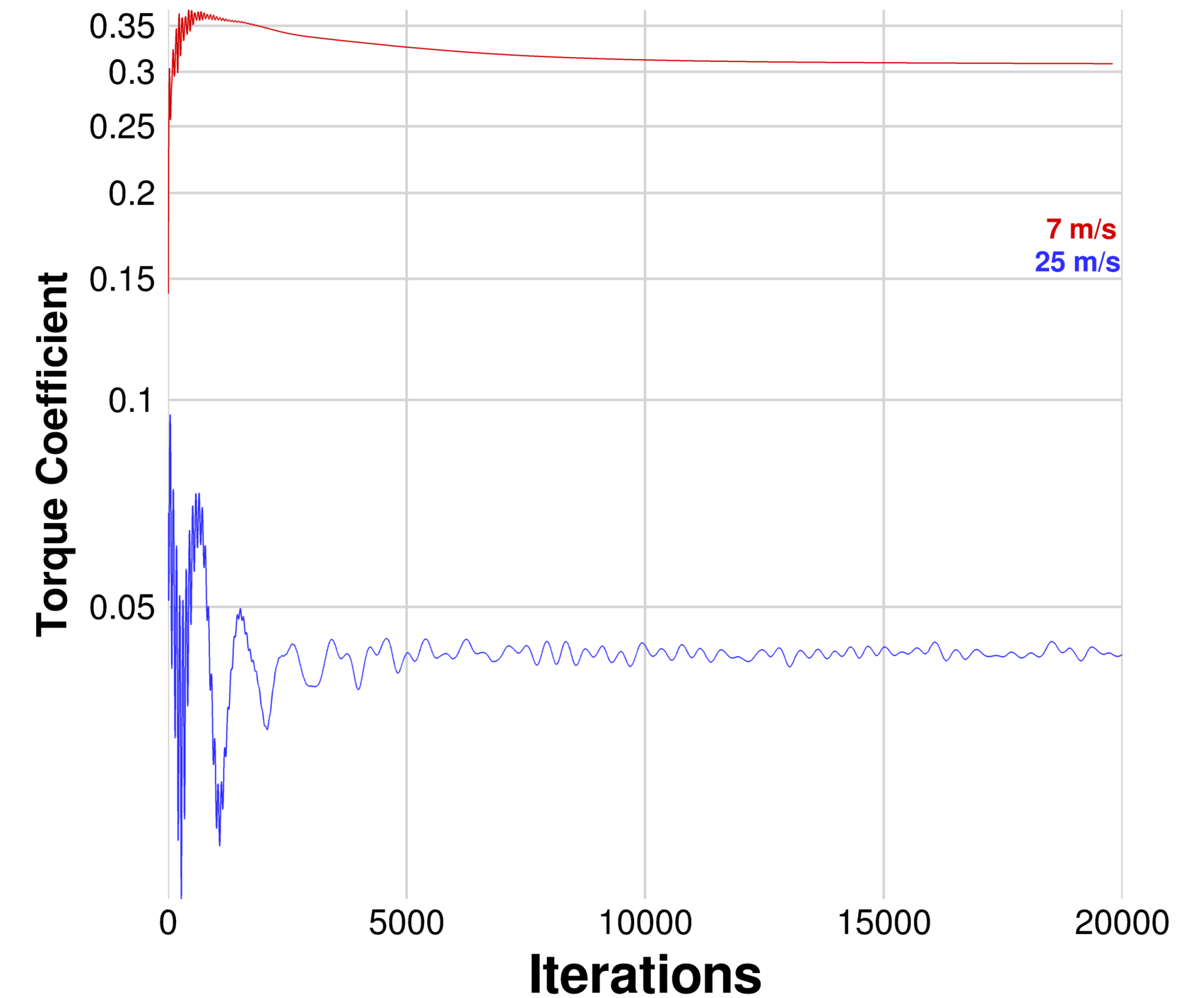
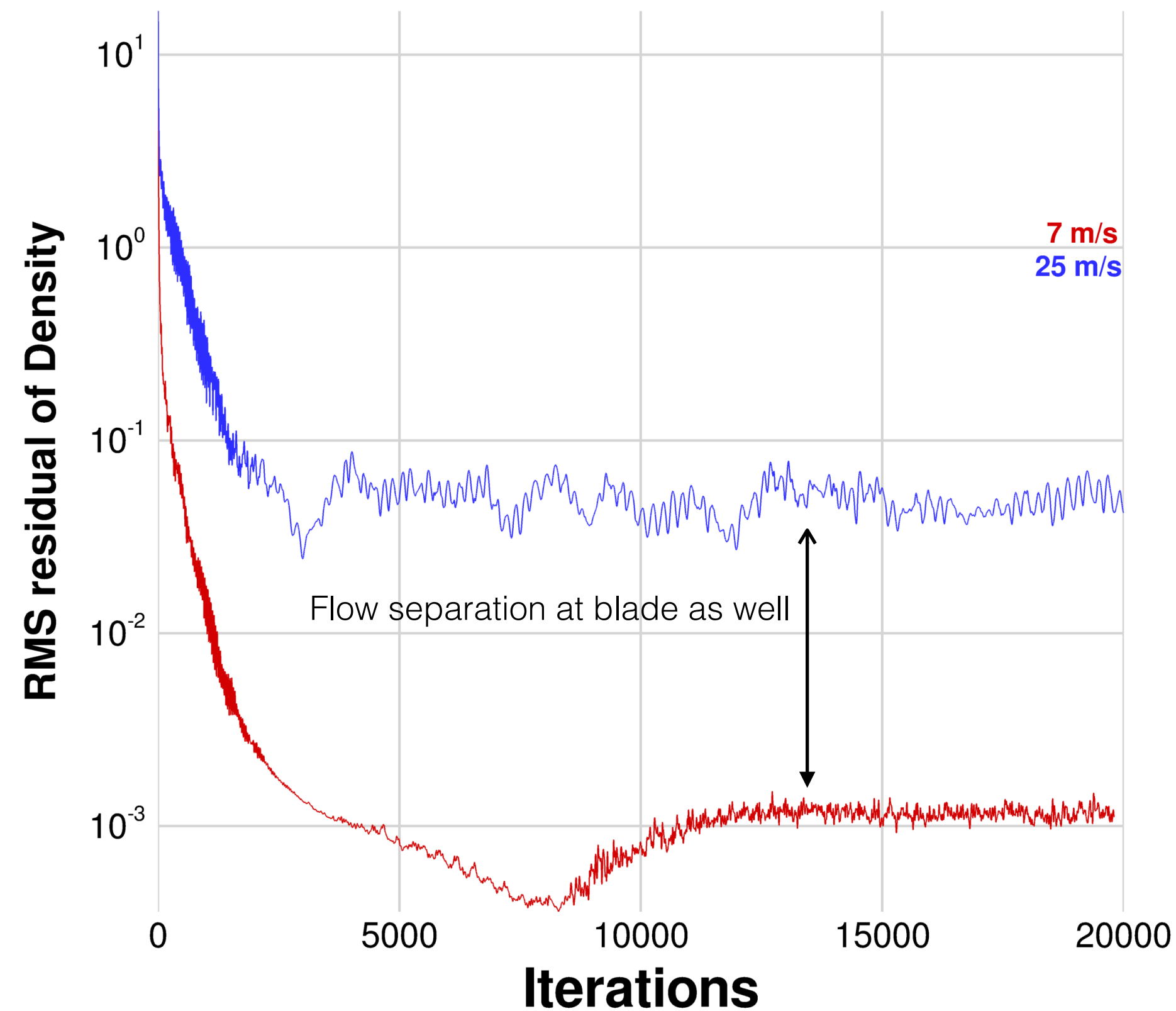


While attached flows are well predicted,  
the separated flow conditions are not





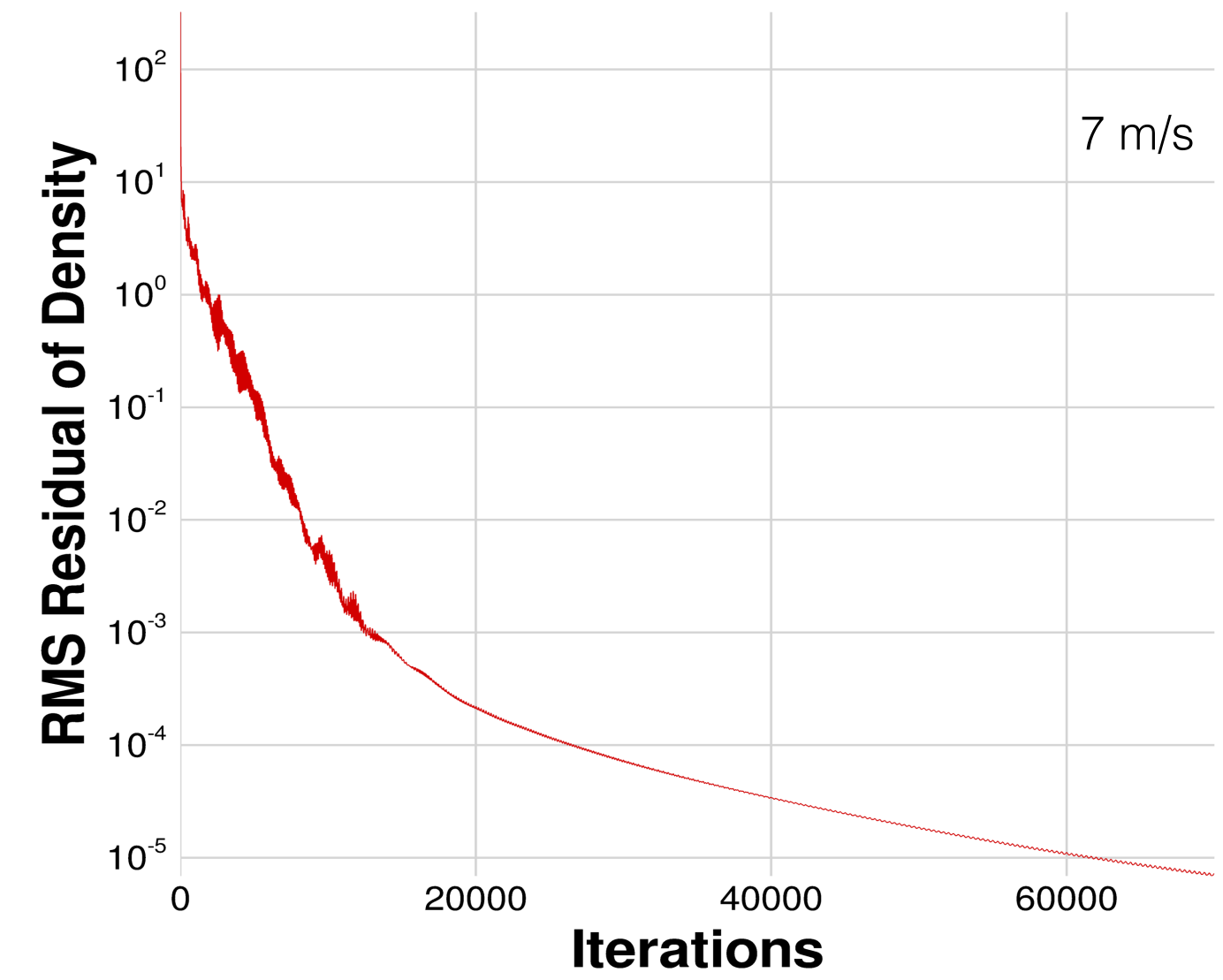
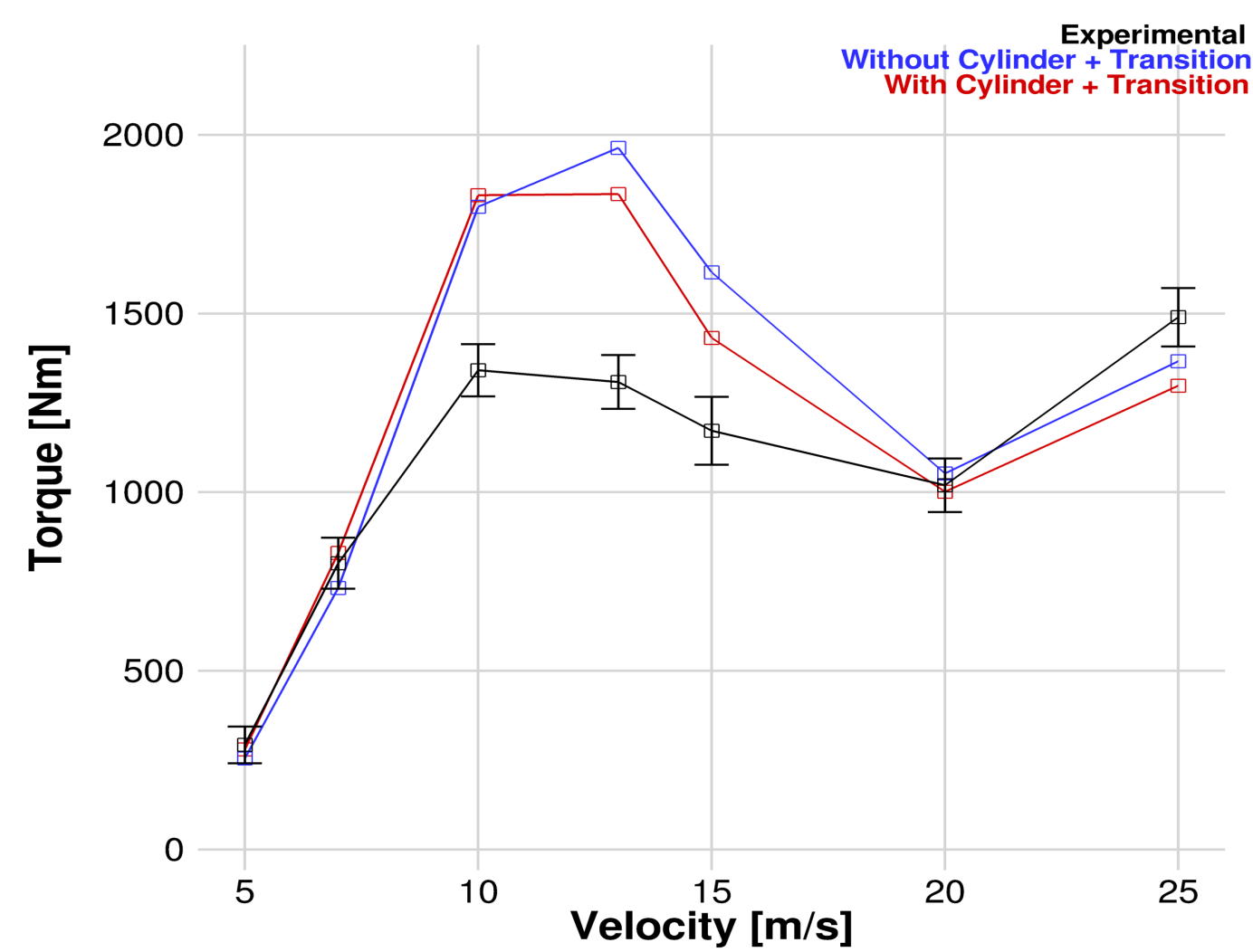
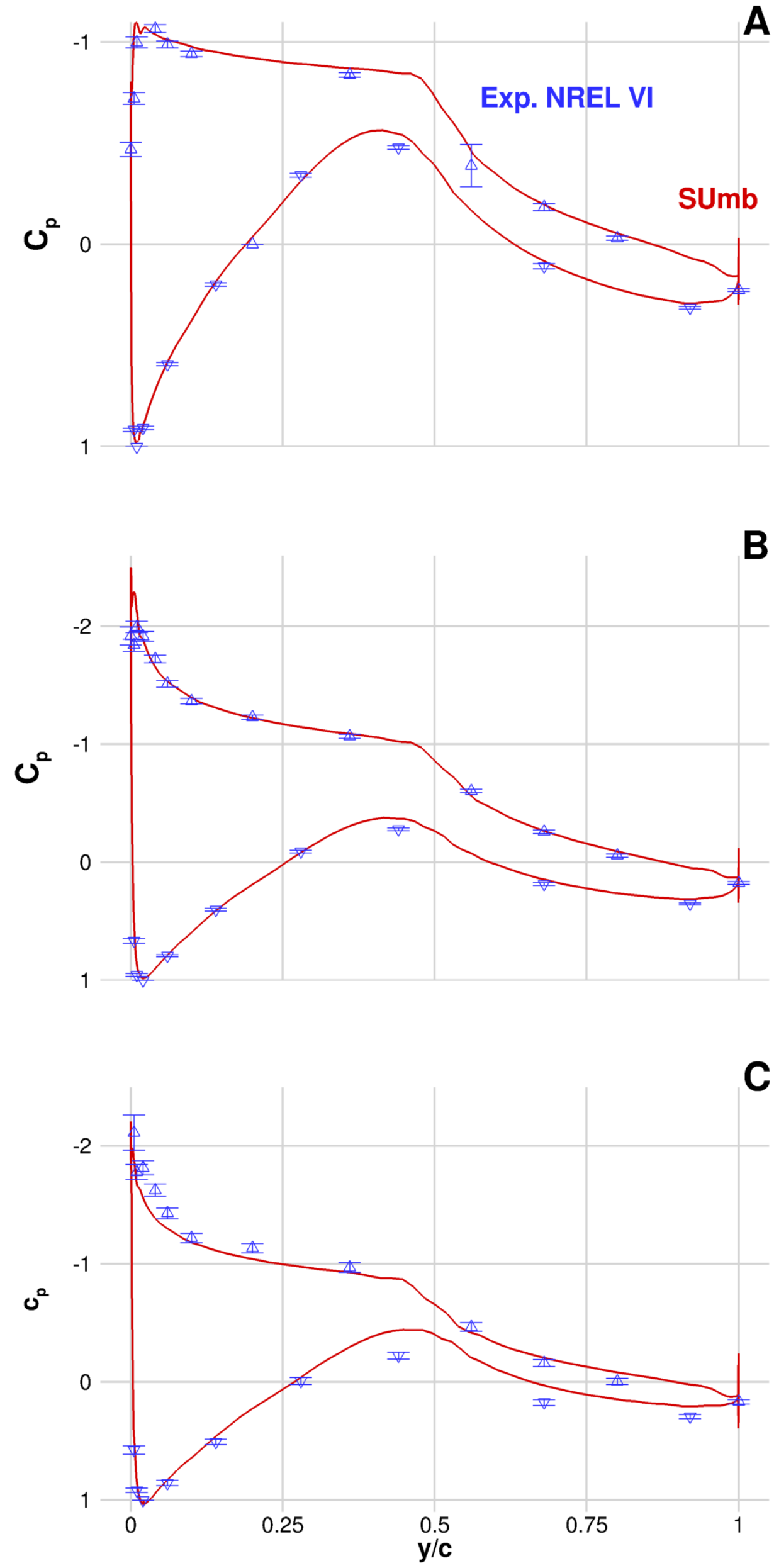
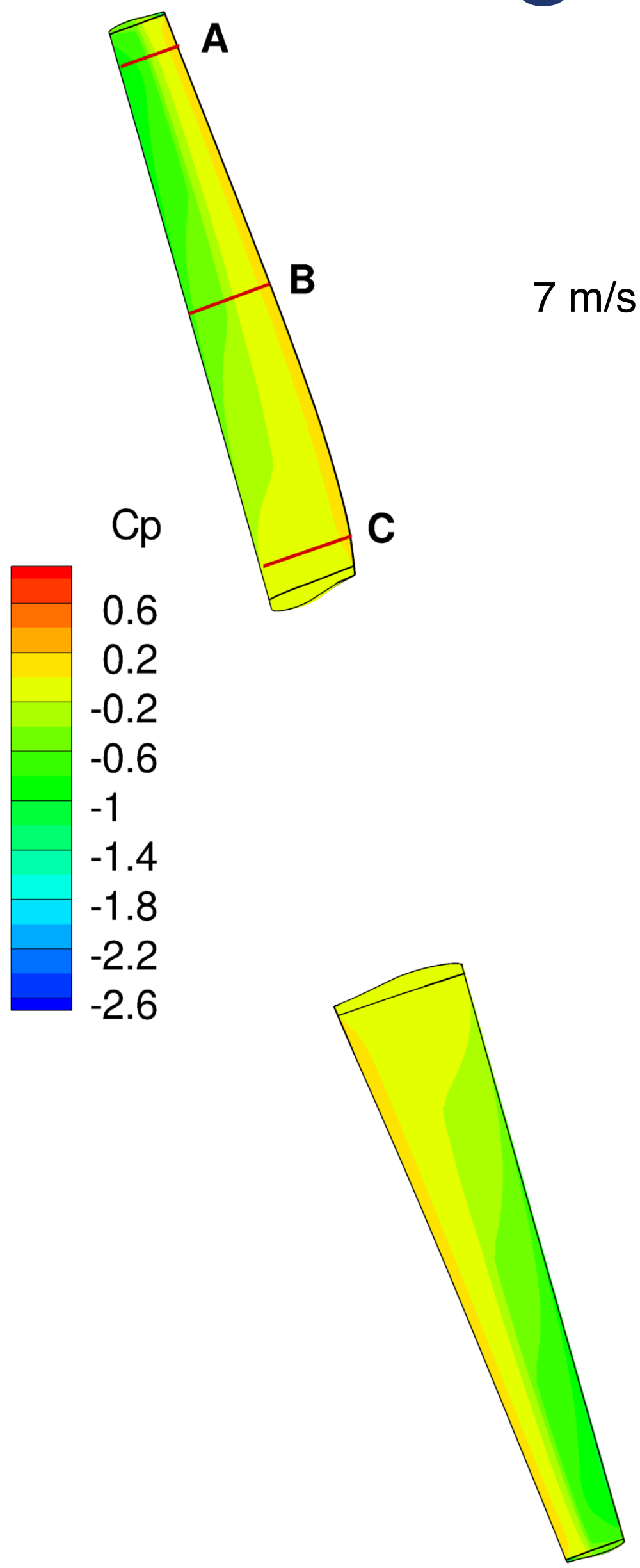
... but stagnation in residuals due to unsteadiness at cylindrical -and transition part



Steady-state adjoint stagnates! —————> No optimization possible



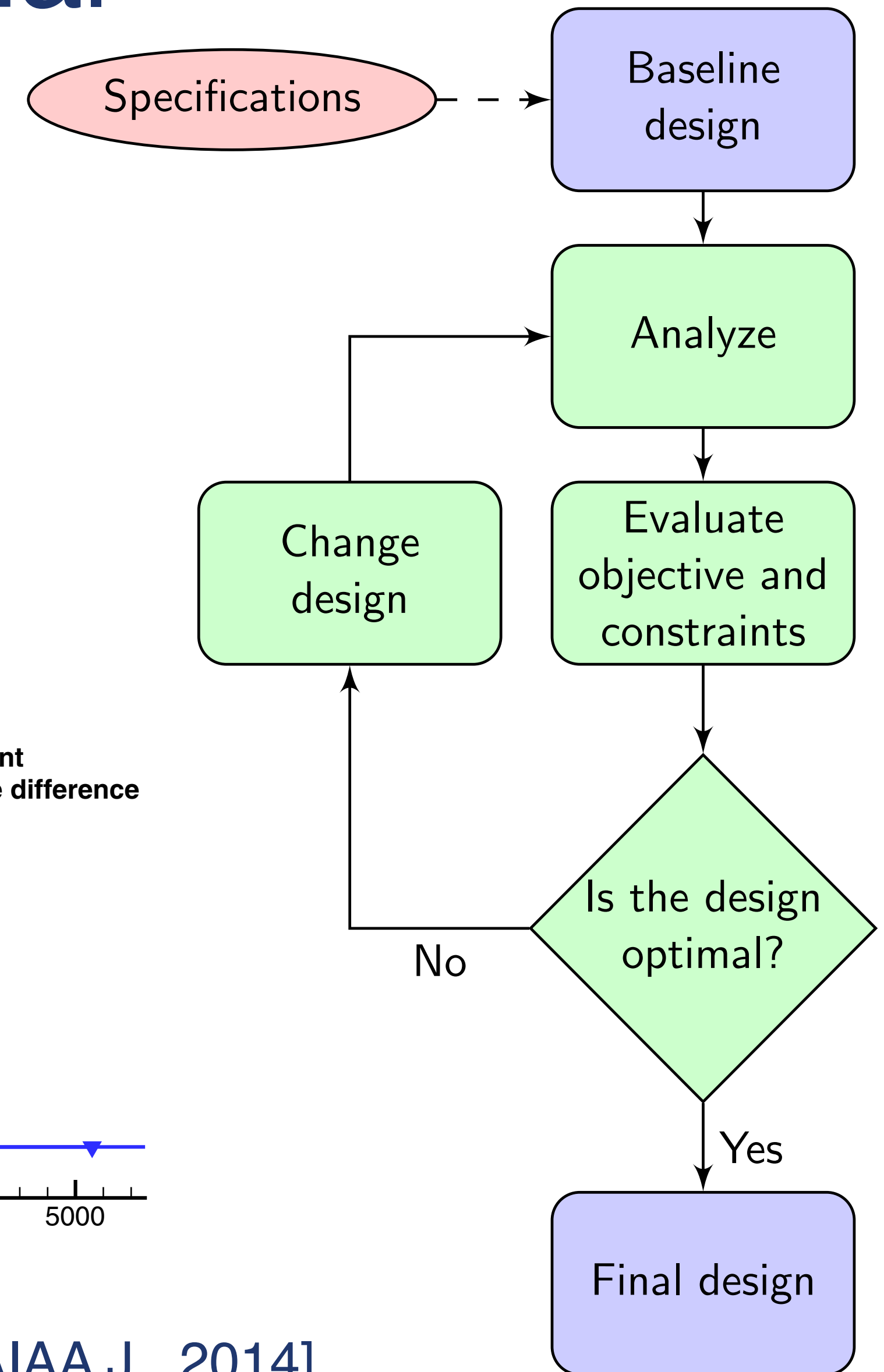
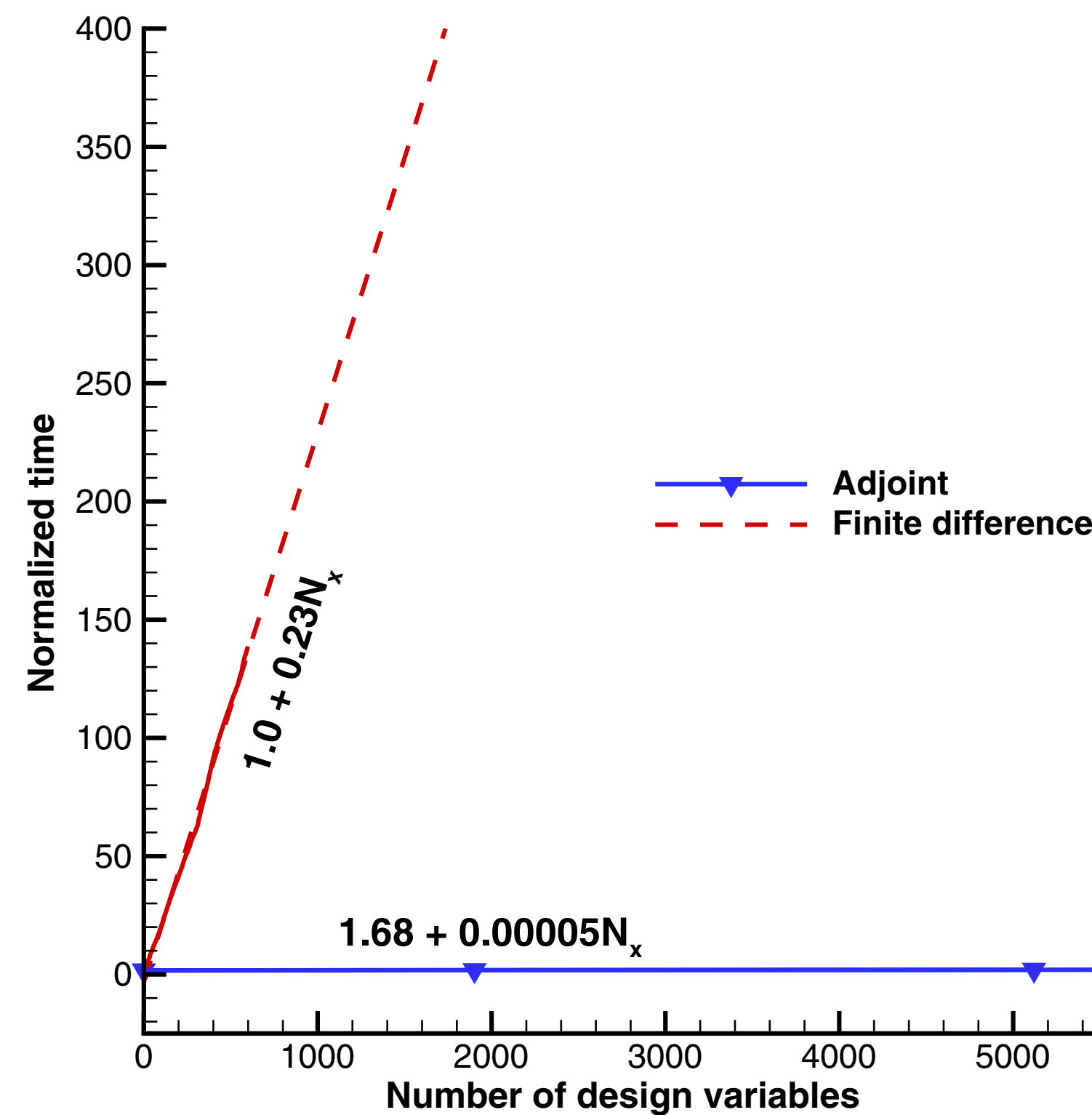
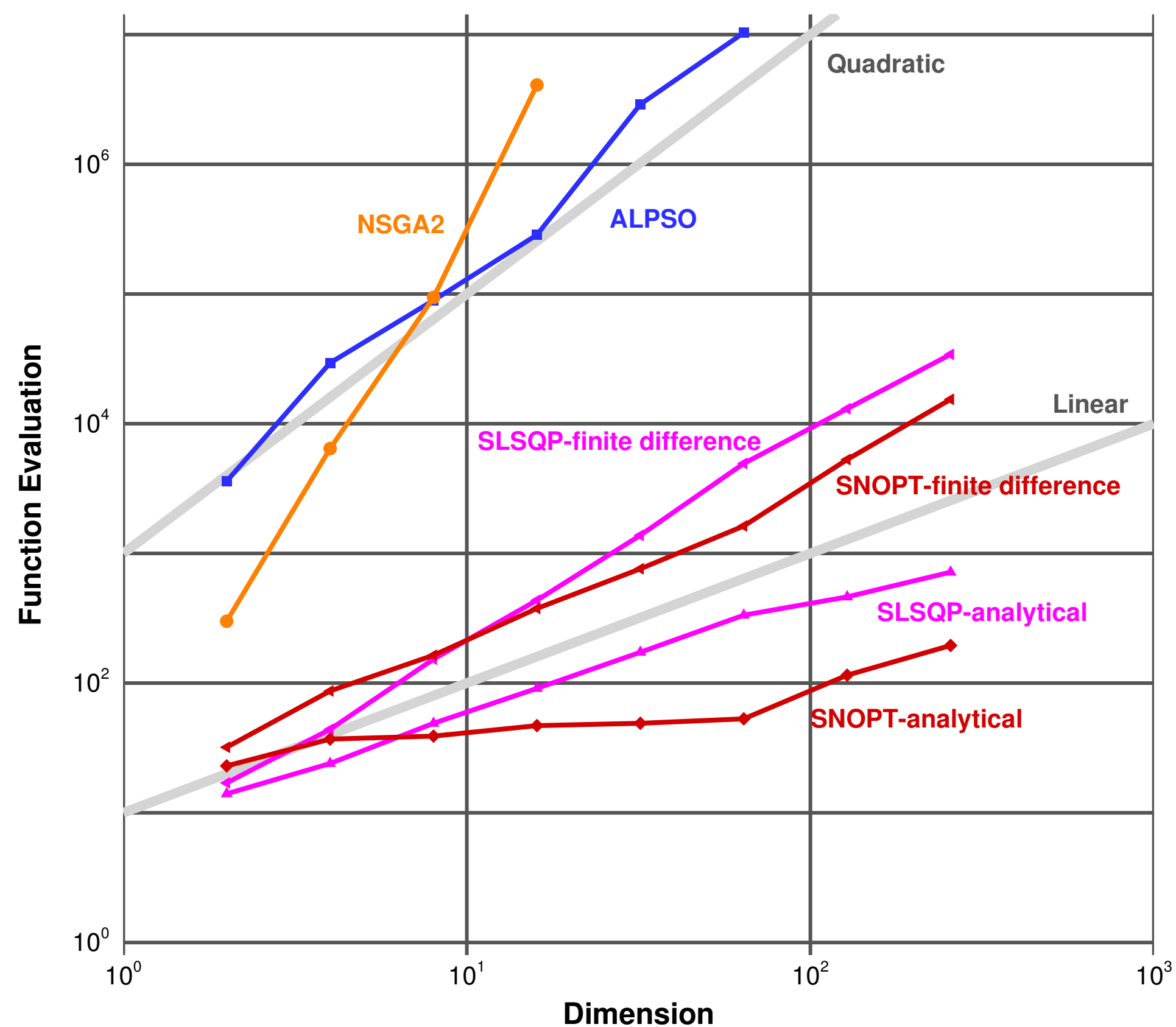
# Removing cylinder and transition part works!



Optimization is feasible in attached flow region



# Gradient-based optimization is essential for large set of design variables

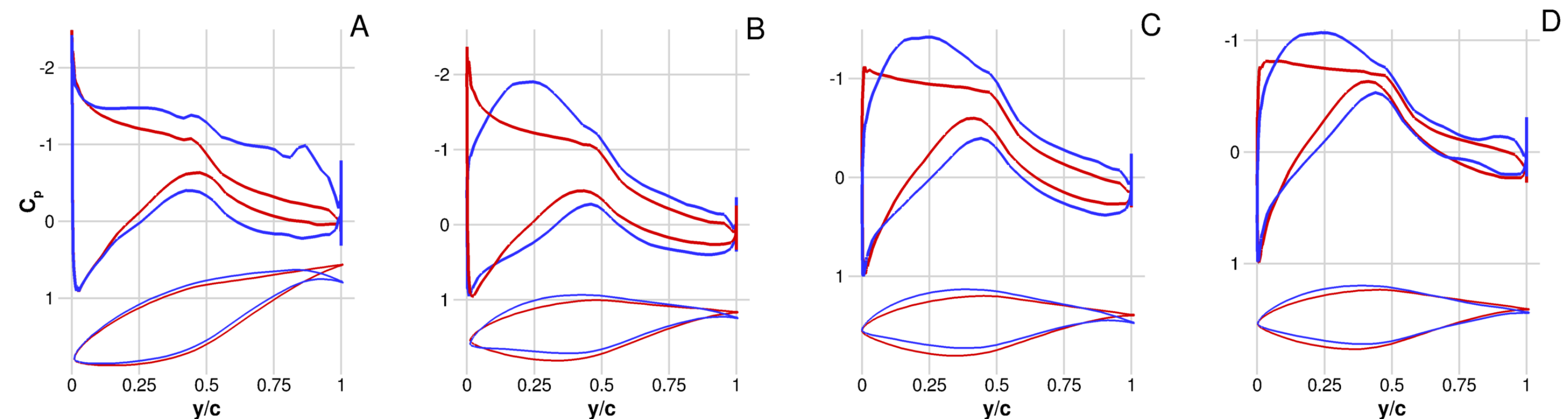
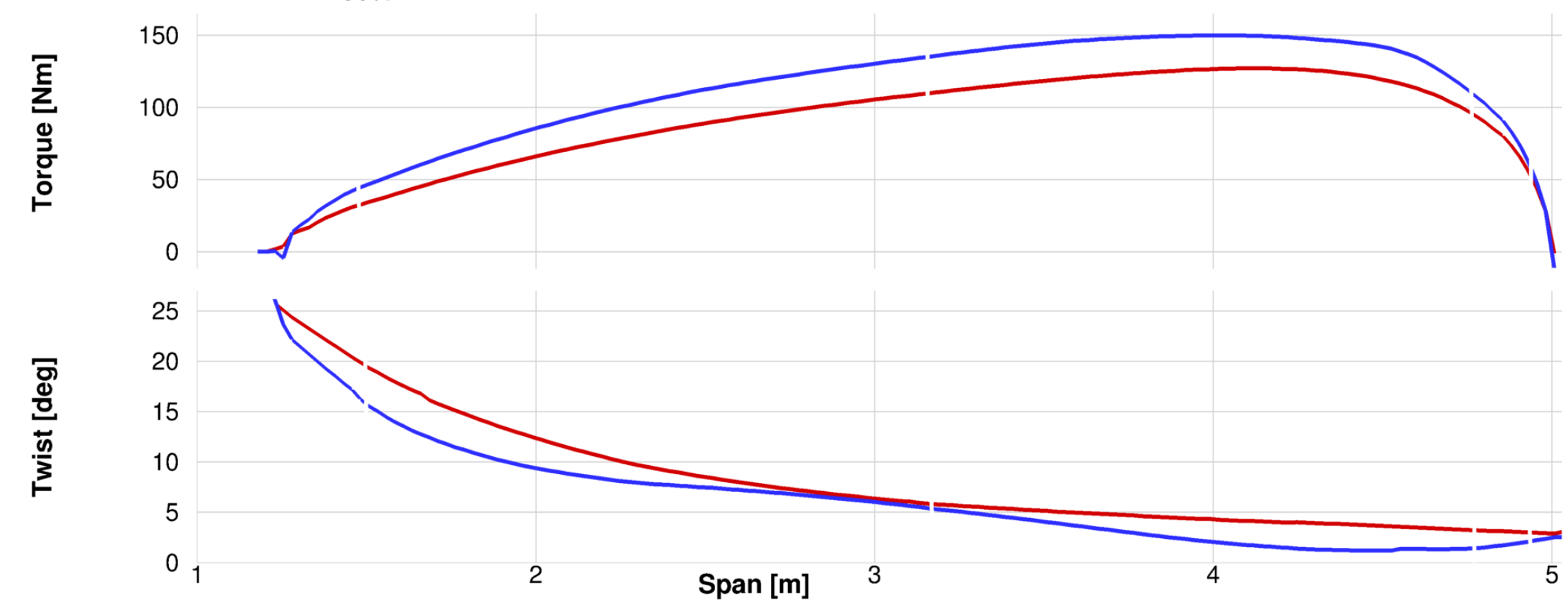
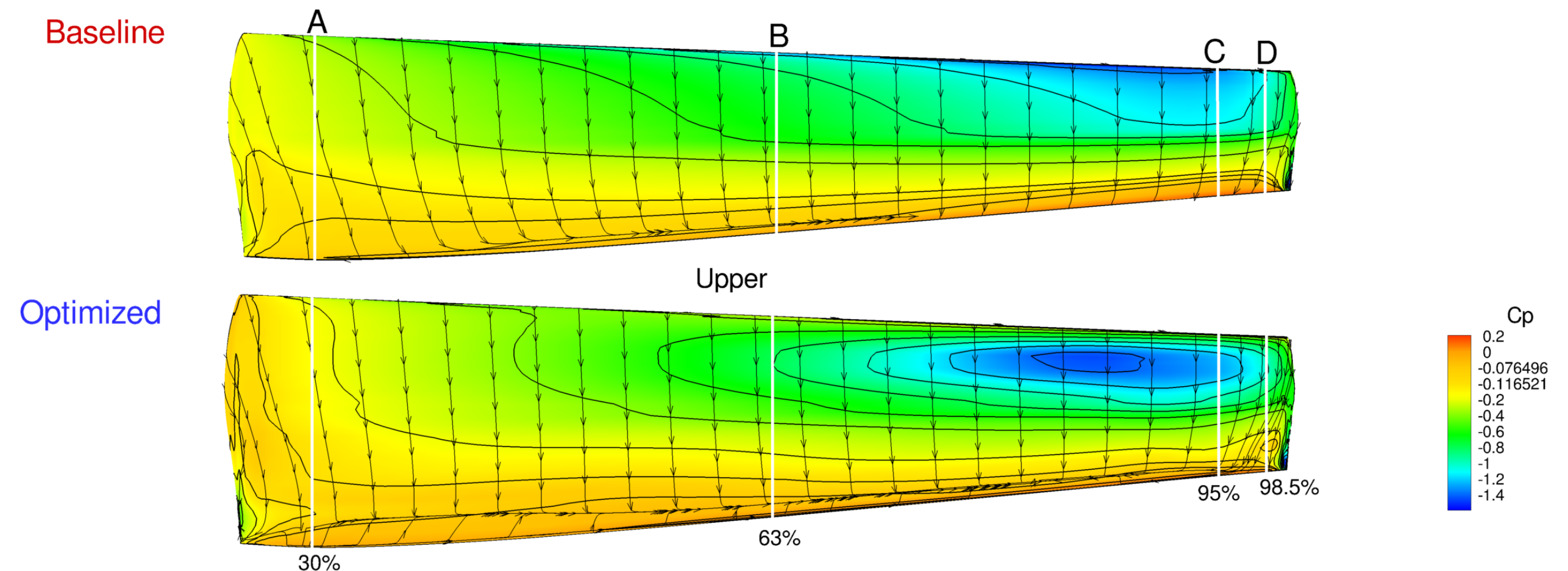
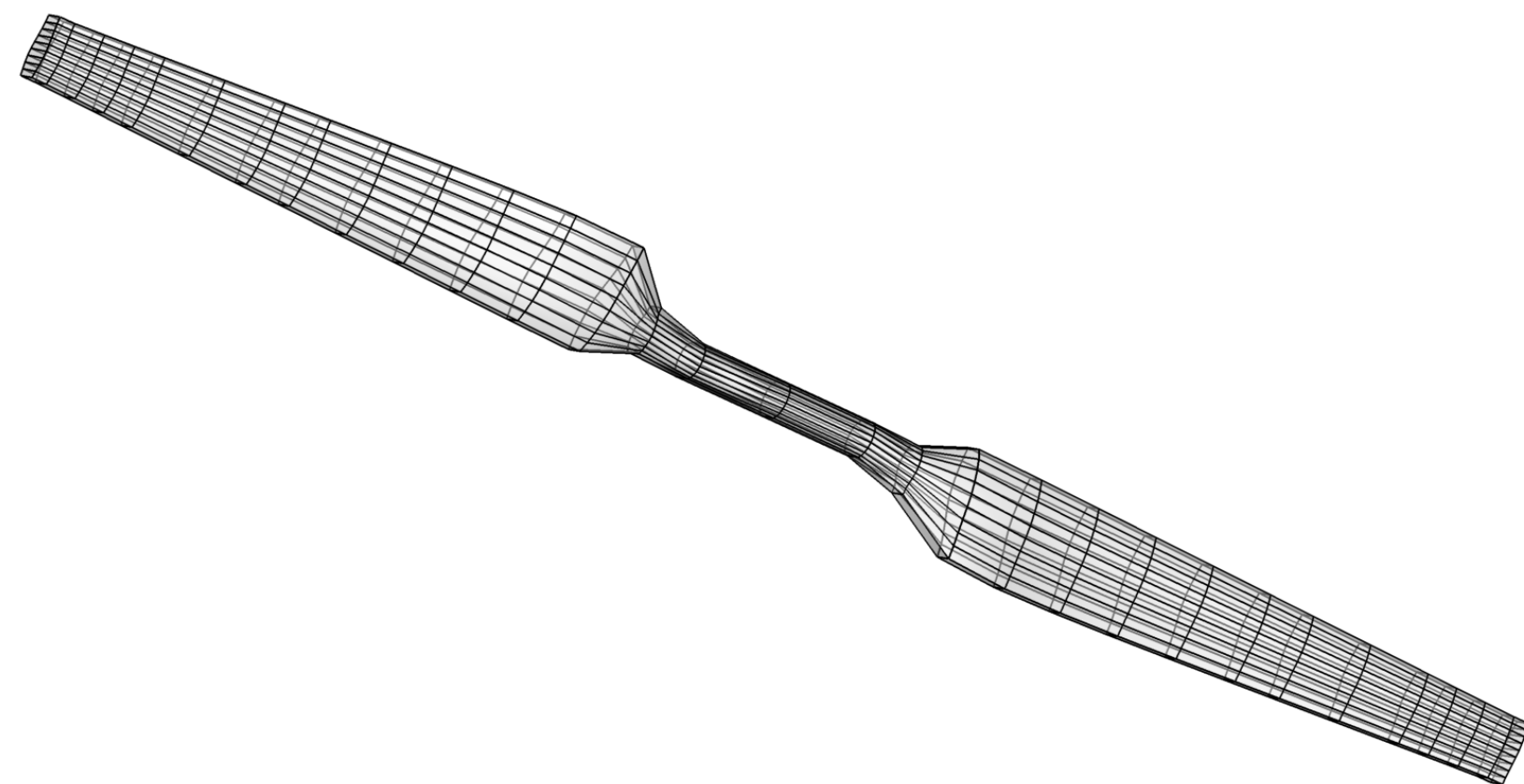


[Kenway, Kennedy, and Martins, AIAA J., 2014]



# 22.4% increase in torque by subtle changes in shape and twist

- Maximizing torque
- 496 design variables: shape and twist
- thickness -and linear constraints

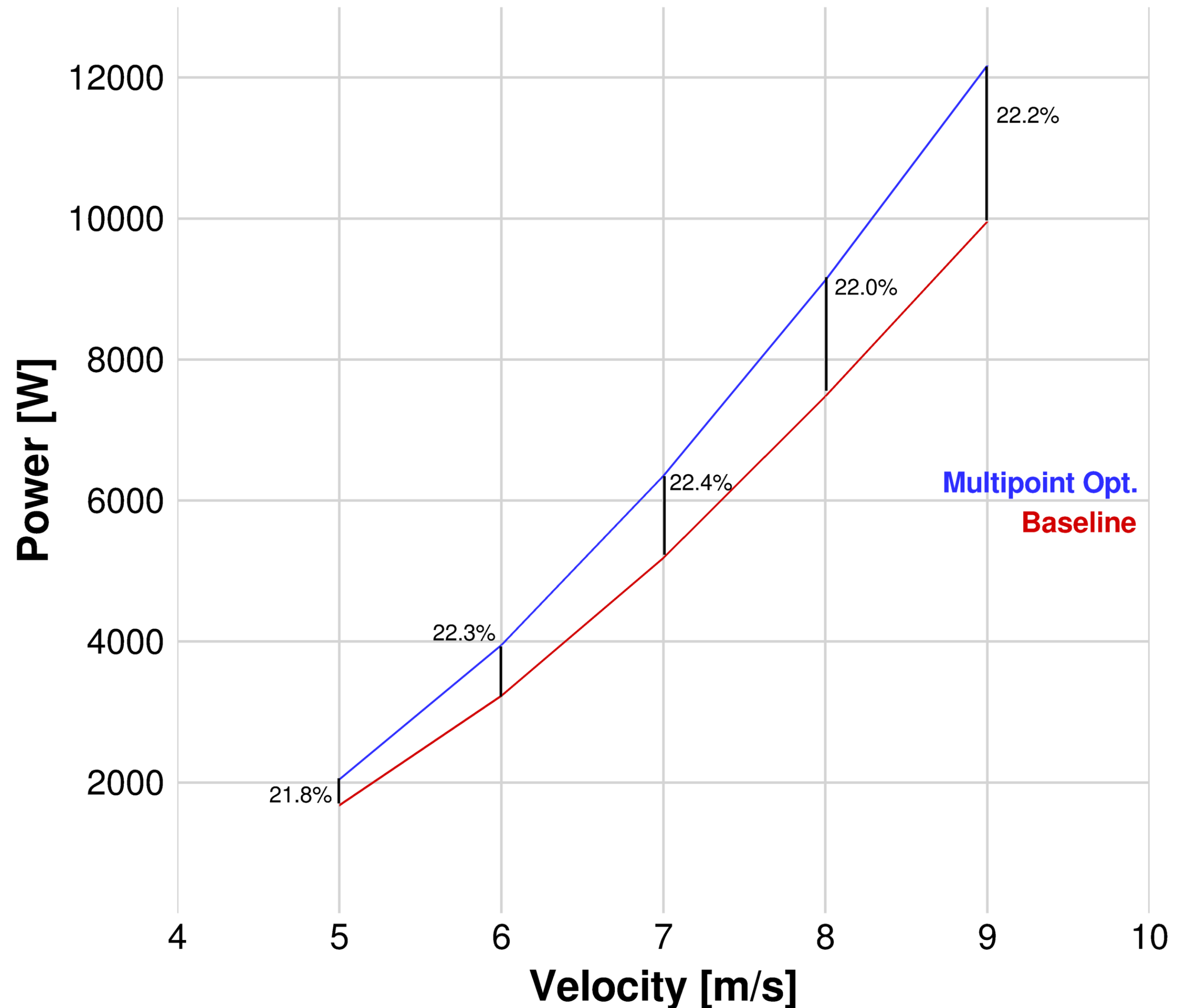




# 26.5% improvement in Annual Energy Production

- Optimize the design for various wind speeds (cut-in to rated wind speeds)
- AEP based on Rayleigh distribution
- Dutch part of the North Sea

AEP Initial : 19.9 MWh  
AEP Optimal: 25.3 MWh





# Summary

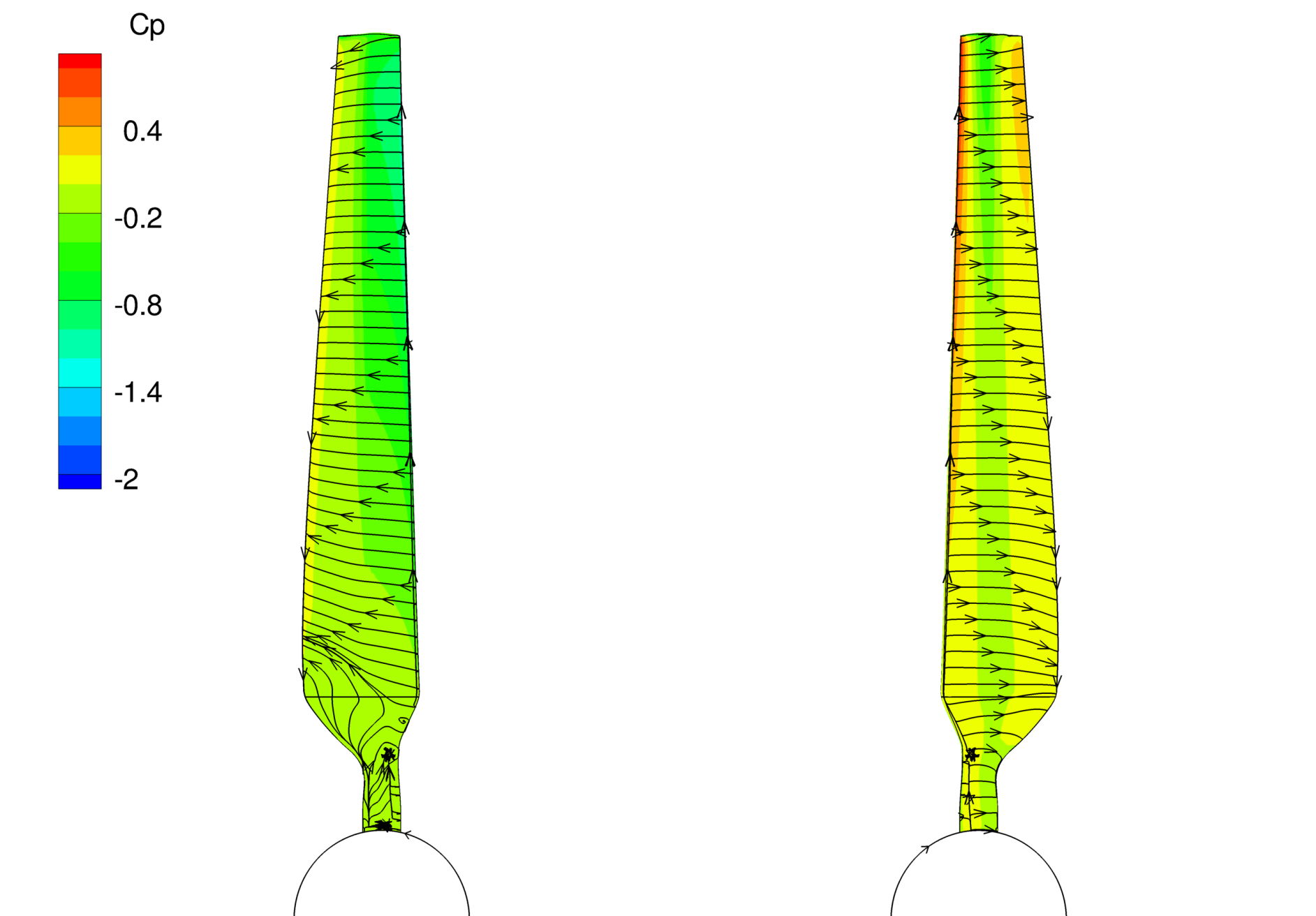
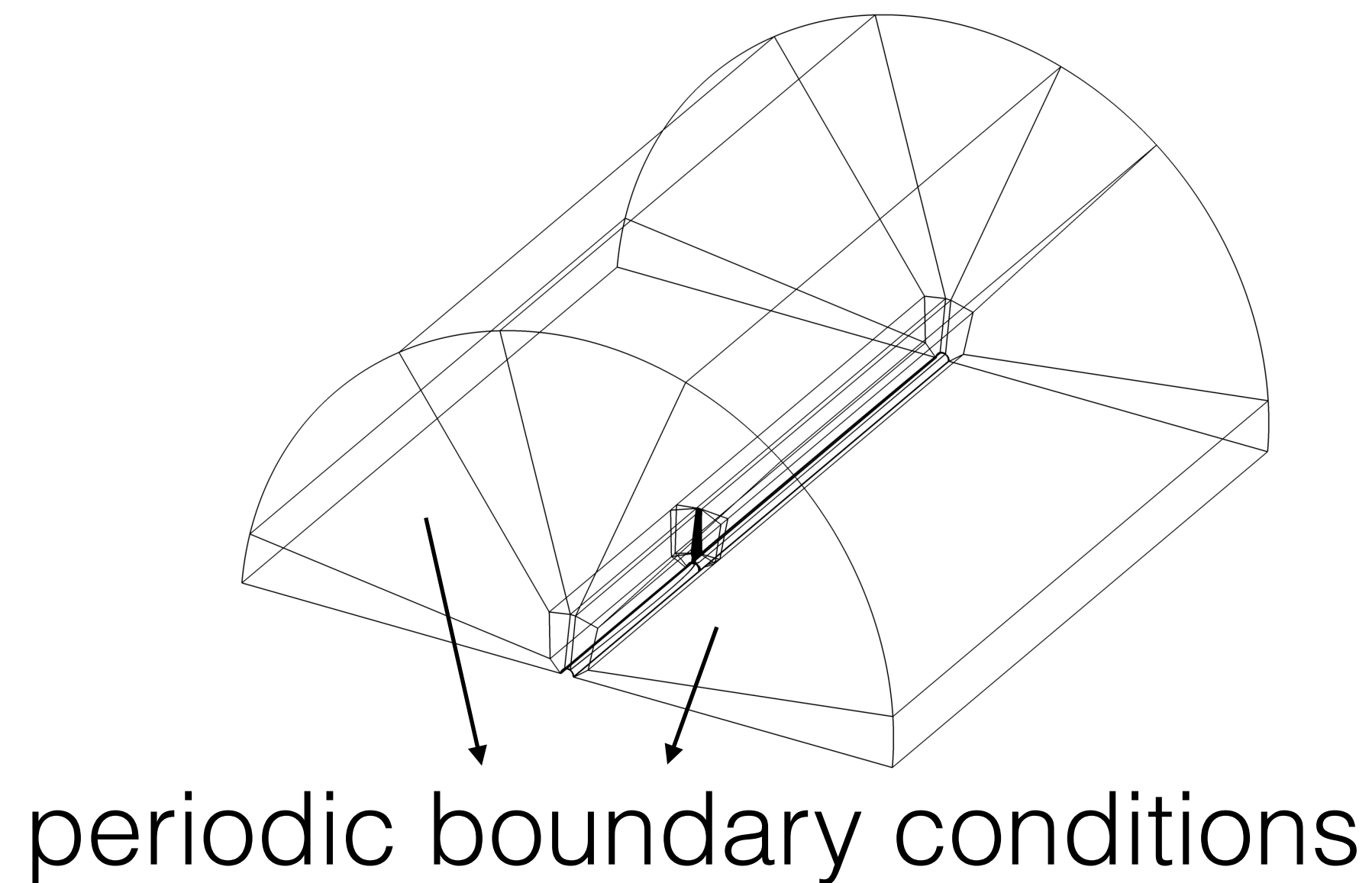
A gradient-based aerodynamic shape optimization methodology is developed for wind turbine blades

- Gradient computation and optimization
- Unsteadiness results currently in non-solvable optimization
- Fast and robust aerodynamic shape optimization



# Future Work

- Unsteady adjoint solver for optimization of quasi-steady solutions
- Mesh perturbation method for periodic boundary conditions
- Adding more design variables (pitch, rotating speed, and planform) and constraints (separation, bending moments) for more realistic designs
- Aerostructural optimization



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